Hazard Mapping of the Philippines Using LIDAR (Phil-LI AR 1)

# LiDAR Surveys and Flood Mapping of Caramay River



University of the Philippines Training Center for Applied Geodesy and Photogrammetry University of the Philippines Los Baños

**APRIL 2017** 

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Published by the UP Training Center for Applied Geodesy and Photogrammetry (TCAGP) College of Engineering University of the Philippines – Diliman Quezon City 1101 PHILIPPINES

E.C. Paringit and E.R. Abucay (eds.) (2017), LiDAR Surveys and Flood Mapping of Caramay River, Quezon City: University of the Philippines Training Center for Applied Geodesy and Photogrammetry-126pp.

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National Library of the Philippines ISBN: 978-621-430-133-1

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## LIST OF ACRONYMS AND ABBREVIATIONS

| AAC     | Asian Aerospace Corporation                                       |
|---------|---|
| Ab      | abutment  |
| ALTM    | Airborne LiDAR Terrain Mapper                                     |
| ARG     | automatic rain gauge  |
| ATQ     | Antique   |
| AWLS    | Automated Water Level Sensor                                      |
| BA      | Bridge Approach   |
| BM      | benchmark   |
| CAD     | Computer-Aided Design   |
| CN      | Curve Number  |
| CSRS    | Chief Science Research Specialist                                 |
| DAC     | Data Acquisition Component  |
| DEM     | Digital Elevation Model   |
| DENR    | Department of Environment and Natural<br>Resources                |
| DOST    | Department of Science and Technology                              |
| DPPC    | Data Pre-Processing Component                                     |
| DREAM   | Disaster Risk and Exposure Assessment for<br>Mitigation [Program] |
| DRRM    | Disaster Risk Reduction and Management                            |
| DSM     | Digital Surface Model   |
| DTM     | Digital Terrain Model   |
| DVBC    | Data Validation and Bathymetry<br>Component                       |
| FMC     | Flood Modeling Component  |
| FOV     | Field of View   |
| GiA     | Grants-in-Aid   |
| GCP     | Ground Control Point  |
| GNSS    | Global Navigation Satellite System                                |
| GPS     | Global Positioning System   |
| HEC-HMS | Hydrologic Engineering Center - Hydrologic<br>Modeling System     |
| HEC-RAS | Hydrologic Engineering Center - River<br>Analysis System          |
| HC      | High Chord  |
| IDW     | Inverse Distance Weighted [interpolation method]                  |

| IMU      | Inertial Measurement Unit  |  |  |  |  |
|----------|--|--|--|--|--|
| kts      | knots  |  |  |  |  |
| LAS      | LiDAR Data Exchange File format  |  |  |  |  |
| LC       | Low Chord  |  |  |  |  |
| LGU      | local government unit  |  |  |  |  |
| Lidar    | Light Detection and Ranging  |  |  |  |  |
| LMS      | LiDAR Mapping Suite  |  |  |  |  |
| m AGL    | meters Above Ground Level  |  |  |  |  |
| MMS      | Mobile Mapping Suite   |  |  |  |  |
| MSL      | mean sea level   |  |  |  |  |
| NSTC     | Northern Subtropical Convergence   |  |  |  |  |
| PAF      | Philippine Air Force   |  |  |  |  |
| PAGASA   | Philippine Atmospheric Geophysical<br>and Astronomical Services<br>Administration            |  |  |  |  |
| PDOP     | Positional Dilution of Precision   |  |  |  |  |
| РРК      | Post-Processed Kinematic [technique]   |  |  |  |  |
| PRF      | Pulse Repetition Frequency   |  |  |  |  |
| PTM      | Philippine Transverse Mercator   |  |  |  |  |
| QC       | Quality Check  |  |  |  |  |
| QT       | Quick Terrain [Modeler]  |  |  |  |  |
| RA       | Research Associate   |  |  |  |  |
| RIDF     | Rainfall-Intensity-Duration-Frequency  |  |  |  |  |
| RMSE     | Root Mean Square Error   |  |  |  |  |
| SAR      | Synthetic Aperture Radar   |  |  |  |  |
| SCS      | Soil Conservation Service  |  |  |  |  |
| SRTM     | Shuttle Radar Topography Mission   |  |  |  |  |
| SRS      | Science Research Specialist  |  |  |  |  |
| SSG      | Special Service Group  |  |  |  |  |
| ТВС      | Thermal Barrier Coatings   |  |  |  |  |
| UPLB     | University of the Philippines Los Baños  |  |  |  |  |
| UP-TCAGP | University of the Philippines – Training<br>Center for Applied Geodesy and<br>Photogrammetry |  |  |  |  |
| UTM      | Universal Transverse Mercator  |  |  |  |  |
| WGS      | World Geodetic System  |  |  |  |  |

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

## CHAPTER 1: OVERVIEW OF THE PROGRAM AND CARAMAY RIVER

Enrico C. Paringit, Dr. Eng., Asst. Prof. Edwin R. Abucay, and Ms. Sandra S. Samantela

#### 1.1 Background of the Phil-LIDAR 1 Program

The University of the Philippines Training Center for Applied Geodesy and Photogrammetry (UP-TCAGP) launched a research program entitled "Nationwide Hazard Mapping using LiDAR" or Phil-LiDAR 1, supported by the Department of Science and Technology (DOST) Grants-in-Aid (GiA) Program. The program was primarily aimed at acquiring a national elevation and resource dataset at sufficient resolution to produce information necessary to support the different phases of disaster management. Particularly, it targeted to operationalize the development of flood hazard models that would produce updated and detailed flood hazard maps for the major river systems in the country.

Also, the program was aimed at producing an up-to-date and detailed national elevation dataset suitable for 1:5,000 scale mapping, with 50 cm and 20 cm horizontal and vertical accuracies, respectively. These accuracies were achieved through the use of the state-of-the-art Light Detection and Ranging (LiDAR) airborne technology procured by the project through DOST.

The implementing partner university for the Phil-LiDAR 1 Program is the University of the Philippines Los Baños (UPLB). UPLB is in charge of processing LiDAR data and conducting data validation reconnaissance, cross section, bathymetric survey, validation, river flow measurements, flood height and extent data gathering, flood modeling, and flood map generation for the 45 river basins in the Southern Luzon region. The university is located in Los Baños in the province of Laguna.

#### 1.2 Overview of the Caramay River Basin

Caramay River Basin, a 15,633-ha watershed, covers the Municipality of Roxas, and a small portion of San Vicente in the province of Palawan. It encompasses barangay Caramay, Jolo, Nicanor Zabala, and Tinitian in the municipality of Roxas; and Caruray in San Vicente. The DENR River Basin Control Office identified the basin to have a drainage area of 69 km<sup>2</sup> and an estimated 110 million cubic meter (MCM) annual run-off (RBCO, 2015).

In terms of geology, the basin area is classified as having Basement Complex (Pre-Jurassic) and Recent. Generally, the slope in the area can be classified as undulating to very steep with elevation ranging from 50 to more than 300 meters above sea level (masl). The soil in the large extent of rough mountainous land is still unclassified. However, other area has San Manuel clay loam and Coron clay loam. Dense vegetation of closed forest (broadleaved) dominates the basin area along with other wooded land (wooded grassland) and built-up area.

Its main stem, Caramay River, is part of the 45 river systems in MIMAROPA. The Caramay river passes through Caramav, Jolo. Nicanor Zabala. Tinitian. According to the 2015 national census of NSO, a total of tributed in Brgy. Caramay,

in the Municipality of Roxas (NSO, 2015).

Fishing is the primary source of livelihood in the Municipality of Roxas since most of the barangays are in coastal areas. Moreover, Brgy. Caramay has been identified as a Marine Protected Area (MPA) focal site by the Palawan Council for Sustainable Development Staff. The MPAs serve as habitats to many aquatic species such as the endangered dugong, green groupers, lobsters, and many more. The campaign aims to educate fishermen with the right fishing methods, and to increase the number of fish in MPAs (PCSD, 2015).



119°10'0"E

Figure 1. Map of Caramay River Basin (in brown)

In the Caramay River Basin area, Climate Type I and III prevails, similar to its larger environment in MIMAROPA and Laguna based on the Modified Corona Classification of climate. Type I has two pronounced seasons, dry from November to April, and wet the rest of the year with maximum rain period from June to September. On the other hand, Type III has no very pronounced maximum rain period and with short dry season lasting only from one to three months, during the period from December to February or from March to May.

During the wet or typhoon season, some communities are affected by flooding in the Caramay River Basin area. The study conducted by the Mines and Geosciences Bureau showed that generally the barangays in the basin area has no susceptibility to flooding except for those small areas near Caramay river that has moderate to high susceptibility. Based on the field surveys conducted by the PHIL-LiDAR 1 validation team, there were two notable weather disturbances that caused flooding in 2005 (Quedan) and 2013 (Yolanda). Last November 2013, before exiting the country, super typhoon Yolanda, internationally known as *Haiyan*, made landfall on the region of Palawan. The Provincial Disaster Risk Reduction of Palawan released a report stating that fourteen (14) municipalities were placed under state of calamity, one of them was the Municipality of Roxas. At least 20,000 families from the municipalities placed under state of calamity were affected by the storm (Rappler.com, 2013). For landslides, all barangays located in the basin particularly the upper sloping areas have moderate to high susceptibility.

2

## CHAPTER 2: LIDAR DATA ACQUISITION OF THE CARAMAY FLOODPLAIN

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The methods applied in this Chapter were based on the DREAM methods manual (Sarmiento, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

#### 2.1 Flight Plans

Plans were made to acquire LiDAR data within the delineated priority area for Caramay Floodplain in Palawan. These missions were planned for 33 lines and ran for at most four and a half (4.5) hours including take-off, landing and turning time. The flight planning parameters for the LiDAR system is found in Table 1. Figure 2 shows the flight plans and base stations for Caramay Floodplain.

Table 1. Parameters used in the Gemini LiDAR System during Flight Acquisition.

| Block Name | Flying<br>Height<br>(m AGL) | Overlap<br>(%) | Max.<br>Field<br>of<br>View<br>(θ) | Pulse Rate<br>Frequency<br>(PRF) (kHz) | Scan<br>Frequency<br>(Hz) | Average<br>Speed<br>(kts) | Average<br>Turn Time<br>(Minutes) |
|------------|-----------------------------|----------------|------------------------------------|--|---------------------------|---------------------------|-----------------------------------|
| BLK40A     | 1200                        | 30             | 30                                 | 125                                    | 50                        | 130                       | 5                                 |
| BLK42A     | 1200                        | 30             | 30                                 | 125                                    | 50                        | 130                       | 5                                 |
| BLK42eA    | 1200                        | 30             | 30                                 | 125                                    | 50                        | 130                       | 5                                 |
| BLK42eB    | 1200                        | 30             | 30                                 | 125                                    | 50                        | 130                       | 5                                 |



Figure 2. Flight plans and base stations used for Caramay Floodplain

#### 2.2 Ground Base Station

The project team was able to recover two (2) NAMRIA ground control points: PLW-23 which is of first (1<sup>st</sup>) order accuracy, and PLW-4030 which is of fourth (4<sup>th</sup>) order accuracy. One (1) NAMRIA benchmark was recovered: PL-267. This benchmark was used as vertical reference point and was also established as ground control point. The certifications for the NAMRIA reference points are found in Annex 2, while the processing report NAMRIA benchmark is found in Annex 3. These were used as base stations during flight operations for the entire duration of the survey (November 18-28, 2015). Base stations were observed using dual frequency GPS receivers, TRIMBLE SPS 852 and SPS R8. Flight plans and location of base stations used during the aerial LiDAR acquisition in Caramay floodplain are shown in Figure 2. The list of team members are shown in Annex 4.

Figure 3 to Figure 5 show the recovered NAMRIA reference points within the area, in addition Table 2 to Table 4 show the details about the following NAMRIA control stations and established points, Table 5 shows the list of all ground control points occupied during the acquisition together with the corresponding dates of utilization.



Figure 3. GPS set-up over PLW-23 as recovered at Jolo Elementary School, Puerto Princesa City (a) and NAMRIA reference point PLW-23 (b) as recovered by the field team.

| Table 2. Details of the recovered NAMRIA horizontal control point PLW-23 |  |
|--|--|
| used as base station for the LiDAR Acquisition.                          |  |

| Station Name   | PLW-23             |                         |  |
|--|--------------------|-------------------------|--|
| Order of Accuracy  | 1 <sup>st</sup>    |                         |  |
| Relative Error (horizontal positioning)                                | 1:100,000          |                         |  |
| Geographic Coordinates, Philippine<br>Reference of 1992 Datum (PRS 92) | Latitude           | 10°5'19.52517" North    |  |
|  | Longitude          | 119°12'33.72062" East   |  |
|  | Ellipsoidal Height | 10.427 meters           |  |
| Grid Coordinates, Philippine Transverse                                | Easting            | 577752.254 meters       |  |
| Mercator Zone 1A (PTM Zone 1A PRS 92)                                  | Northing           | 1115630.596 meters      |  |
| Geographic Coordinates, World Geodetic<br>System 1984 Datum (WGS 84)   | Latitude           | 10° 5'15.04804" North   |  |
|  | Longitude          | 119° 12' 39.01413" East |  |
|  | Ellipsoidal Height | 61.07260 meters         |  |
| Grid Coordinates, Universal Transverse                                 | Easting            | 742130.31 meters        |  |
| 92)  | Northing           | 1115973.89 meters       |  |



Figure 4. GPS set-up over PLW-4030 as recovered on the ground beside Jolo Bridge, Roxas, Palawan (a) and NAMRIA reference point PLW-4030 (b) as recovered by the field team.

| Table 3. Details of the recovered NAMRIA horizontal control point PLW-4030 |
|--|
| used as base station for the LiDAR Acquisition.                            |

| Station Name   |                    | PLW-4030                |  |
|--|--------------------|-------------------------|--|
| Order of Accuracy  | 4th                |                         |  |
| Relative Error (horizontal positioning)  | 1:10,000           |                         |  |
| Geographic Coordinates, Philippine<br>Reference of 1992 Datum (PRS 92)           | Latitude           | 10° 4' 56.95146" North  |  |
|  | Longitude          | 119° 12' 22.75168" East |  |
|  | Ellipsoidal Height | 11.183 meters           |  |
| Grid Coordinates, Philippine Transverse<br>Mercator Zone 1A (PTM Zone 1A PRS 92) | Easting            | 84042.662 meters        |  |
|  | Northing           | 1116875.986 meters      |  |
| Geographic Coordinates, World Geodetic<br>System 1984 Datum (WGS 84)             | Latitude           | 10° 4′ 52.47562″ North  |  |
|  | Longitude          | 119° 12' 28.04576" East |  |
|  | Ellipsoidal Height | 61.835 meters           |  |



Figure 5. GPS set-up over PL-267 as recovered on the ground beside Itabiak Bridge, Roxas, Palawan (a) and NAMRIA reference point PL-267 (b) as recovered by the field team.

| Table 4. Details of the recovered NAMRIA vertical control point PL-267 |  |
|--|--|
| used as base station for the LiDAR Acquisition.                        |  |

| Station Name   | PL-267             |                         |  |
|--|--------------------|-------------------------|--|
| Order of Accuracy  | 2 <sup>nd</sup>    |                         |  |
| Relative Error (horizontal positioning)                                | 1:50,000           |                         |  |
|  | Latitude           | 10° 30' 40.21529" North |  |
| Geographic Coordinates, Philippine<br>Reference of 1992 Datum (PRS 92) | Longitude          | 119° 21' 48.02348" East |  |
|  | Ellipsoidal Height | 34.545 meters           |  |
|  | Latitude           | 101820.908 meters       |  |
| Geographic Coordinates, World Geodetic<br>System 1984 Datum (WGS 84)   | Longitude          | 1164164.984 meters      |  |
|  | Ellipsoidal Height | 10° 30′ 35.64621″ North |  |
| Grid Coordinates, Universal Transverse                                 | Easting            | 119° 21' 53.27911" East |  |
| 92)  | Northing           | 84.611 meters           |  |

Table 5. Ground Control Points used during LiDAR Data Acquisition

| Date Surveyed | Flight Number | Mission Name    | Ground Control Points       |
|---------------|---------------|-----------------|-----------------------------|
| 18-Nov-15     | 3505G         | 2BLK42AES322A   | PLW-23, PLW-4030            |
| 18-Nov-15     | 3507G         | 2BLK42ISLAS322B | PLW-23, PLW-4030            |
| 20-Nov-15     | 3513G         | 2BLK42islAs324A | PLW-23, PLW-4030            |
| 21-Nov-15     | 3517G         | 2BLK42B325A     | PLW-23, PLW-4030            |
| 28-Nov-15     | 3545G         | 2BLK42B332A     | PL-267, PLW-23,<br>PLW-4030 |

#### 2.3 Flight Missions

Five (5) missions were conducted to complete the LiDAR Data Acquisition in Caramay Floodplain, for a total of sixteen hours and forty-three minutes (16+43) of flying time for RP-C9022. All missions were acquired using the Gemini LiDAR system. Table 6 shows the total area of actual coverage and the corresponding flying hours per mission, while Table 7 presents the actual parameters used during the LiDAR data acquisition.

| Date      | Flight | Flight<br>Plan | Surveyed   | Area<br>Surveyed<br>within the | Area<br>Surveyed<br>Outside the | No. of<br>Images | Flying | Hours |
|-----------|--------|----------------|------------|--------------------------------|---------------------------------|------------------|--------|-------|
| Surveyed  | Number | Area<br>(km2)  | Area (km2) | Floodplain<br>(km2)            | Floodplain<br>(km2)             | (Frames)         | Hr     | Min   |
| 18-Nov-15 | 3505G  | 214.12         | 99.41      | 8.59                           | 90.82                           | NA               | 3      | 35    |
| 18-Nov-15 | 3507G  | 117.39         | 169.79     | 13.65                          | 156.14                          | NA               | 3      | 0     |
| 20-Nov-15 | 3513G  | 117.39         | 210.88     | 13.66                          | 197.22                          | 240              | 4      | 10    |
| 21-Nov-15 | 3517G  | 62.78          | 21.82      | 0.46                           | 21.36                           | 65               | 2      | 18    |
| 28-Nov-15 | 3545G  | 114.31         | 95.67      | 0.54                           | 95.13                           | NA               | 3      | 40    |
| тот       | AL     | 625.99         | 597.57     | 36.9                           | 560.67                          | 305              | 16     | 43    |

Table 6. Flight missions for LiDAR data acquisition in Caramay Floodplain

Table 7. Actual parameters used during LiDAR data acquisition

| Flight<br>Number | Flying<br>Height<br>(m AGL) | Overlap<br>(%) | FOV (θ) | PRF<br>(kHz) | Scan<br>Frequency<br>(Hz) | Average<br>Speed<br>(kts) | Average<br>Turn Time<br>(Minutes) |
|------------------|-----------------------------|----------------|---------|--------------|---------------------------|---------------------------|-----------------------------------|
| 3505G            | 1000, 600                   | 30             | 26, 40  | 100, 125     | 50, 40                    | 120                       | 5                                 |
| 3507G            | 600, 1100                   | 30             | 50, 24  | 125, 100     | 40, 50                    | 120                       | 5                                 |
| 3513G            | 1100, 1200                  | 30             | 24      | 100          | 50                        | 120                       | 5                                 |
| 3517G            | 1100, 900                   | 30             | 24, 30  | 100          | 50                        | 120                       | 5                                 |
| 3545G            | 1100, 850                   | 30             | 24, 40  | 100, 125     | 50                        | 120                       | 5                                 |

#### 2.4. Survey Coverage

Caramay floodplain is located in the province of Palawan with majority of the floodplain situated within the municipality of Roxas. Municipality of Roxas is mostly covered by the survey. The list of municipalities and cities surveyed with at least one (1) square kilometer coverage, is shown in Table 8. The actual coverage of the LiDAR acquisition for Caramay floodplain is presented in Figure 6.

Table 8. List of municipalities and cities surveyed during Caramay Floodplain LiDAR survey.

| Province | Municipality/City    | Area of<br>Municipality/City<br>(km2) | Total Area<br>Surveyed<br>(km2) | Percentage of Area<br>Surveyed |
|----------|----------------------|---------------------------------------|---------------------------------|--------------------------------|
|          | Puerto Princesa City | 2186.36                               | 28.94                           | 1.32%                          |
| Deleuven | Roxas                | 1007.73                               | 109.3                           | 10.85%                         |
| Palawan  | San Vicente          | 870.45                                | 2.89                            | 0.33%                          |
|          | Taytay               | 1325                                  | 38.52                           | 2.91%                          |
|          | Total                | 5389.54                               | 179.65                          | 3.85%                          |



Figure 6. Actual LiDAR survey coverage for Caramay Floodplain.

## CHAPTER 3: LIDAR DATA PROCESSING OF THE CARAMAY FLOODPLAIN

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The methods applied in this Chapter were based on the DREAM methods manual (Ang, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

#### 3.1 Overview of the LIDAR Data Pre-Processing

The data transmitted by the Data Acquisition Component are checked for completeness based on the list of raw files required to proceed with the pre-processing of the LiDAR data. Upon acceptance of the LiDAR field data, georeferencing of the flight trajectory is done in order to obtain the exact location of the LiDAR sensor when the laser was shot. Point cloud georectification is performed to incorporate correct position and orientation for each point acquired. The georectified LiDAR point clouds are subject for quality checking to ensure that the required accuracies of the program, which are the minimum point density, vertical and horizontal accuracies, are met. The point clouds are then classified into various classes before generating Digital Elevation Models such as Digital Terrain Model and Digital Surface Model.

Using the elevation of points gathered in the field, the LiDAR-derived digital models are calibrated. Portions of the river that are barely penetrated by the LiDAR system are replaced by the actual river geometry measured from the field by the Data Validation and Bathymetry Component. LiDAR acquired temporally are then mosaicked to completely cover the target river systems in the Philippines. Orthorectification of images acquired simultaneously with the LiDAR data is done through the help of the georectified point clouds and the metadata containing the time the image was captured.

These processes are summarized in the flowchart shown in Figure 7.



Figure 7. Schematic Diagram for Data Pre-Processing Component

#### 3.2 Transmittal of Acquired LiDAR Data

Data transfer sheets for all the LiDAR missions for Caramay floodplain can be found in Annex 5. Missions flown during the survey conducted on November 2015 used the Airborne LiDAR Terrain Mapper (ALTM<sup>™</sup> Optech Inc.) Gemini system over Roxas, Palawan.

The Data Acquisition Component (DAC) transferred a total of 57.17 Gigabytes of Range data, 1.46 Gigabytes of POS data, 34.39 Megabytes of GPS base station data, and 0 Gigabytes of raw image data to the data server on December 8, 2015. The Data Pre-processing Component (DPPC) verified the completeness of the transferred data. The whole dataset for Caramay was fully transferred on December 8, 2015, as indicated on the Data Transfer Sheets for Caramay floodplain.

#### 3.3 Trajectory Computation

The Smoothed Performance Metrics of the computed trajectory for flight 3507G, one of the Caramay flights, which is the North, East, and Down position RMSE values are shown in Figure 8. The x-axis corresponds to the time of flight, which is measured by the number of seconds from the midnight of the start of the GPS week, which on that week fell on November 15, 2015 00:00AM. The y-axis is the RMSE value for that particular position.



Figure 8. Smoothed Performance Metrics of Caramay Flight 3507G.

The time of flight was from 285000 seconds to 293000 seconds, which corresponds to morning of November 18, 2015. The initial spike that is seen on the data corresponds to the time that the aircraft was getting into position to start the acquisition, and the POS system starts computing for the position and orientation of the aircraft. Redundant measurements from the POS system quickly minimized the RMSE value of the positions. The periodic increase in RMSE values from an otherwise smoothly curving RMSE values correspond to the turn-around period of the aircraft, when the aircraft makes a turn to start a new flight line. Figure 8 shows that the North position RMSE peaks at 0.80 centimeters, the East position RMSE peaks at 0.40 centimeters, and the Down position RMSE peaks at 1.20 centimeters, which are within the prescribed accuracies described in the methodology.



Figure 9. Solution Status Parameters of Caramay Flight 3507G.

The Solution Status parameters of flight 3507G, one of the Caramay flights, which are the number of GPS satellites, Positional Dilution of Precision (PDOP), and the GPS processing mode used, are shown in Figure 9. The graphs indicate that the number of satellites during the acquisition did not go down to 6. Majority of the time, the number of satellites tracked was between 7 and 10. The PDOP value also did not go above the value of 4, which indicates optimal GPS geometry. The processing mode stayed at the value of 0 for majority of the survey with some peaks up to 2 attributed to the turns performed by the aircraft. The value of 0 corresponds to a Fixed, Narrow-Lane mode, which is the optimum carrier-cycle integer ambiguity resolution technique available for POSPAC MMS. All of the parameters adhered to the accuracy requirements for optimal trajectory solutions, as indicated in the methodology. The computed best estimated trajectory for all Caramay flights is shown in Figure 10.



Figure 10. Best Estimated Trajectory for Caramay Floodplain.

#### 3.4 LiDAR Point Cloud Computation

The produced LAS data contains 24 flight lines, with each flight line containing one channel, since the Gemini system contains one channel only. The summary of the self-calibration results obtained from LiDAR processing in LiDAR Mapping Suite (LMS) software for all flights over Caramay floodplain are given in Table 9.

| Parameter  | Acceptable Value | Computed Value |
|--|------------------|----------------|
| Boresight Correction stdev                               | (<0.001degrees)  | 0.000835       |
| IMU Attitude Correction Roll and Pitch Corrections stdev | (<0.001degrees)  | 0.000924       |
| GPS Position Z-correction stdev                          | (<0.01meters)    | 0.0096         |

Table 9. Self-Calibration Results values for Caramay flights.

The optimum accuracy is obtained for all Caramay flights based on the computed standard deviations of the corrections of the orientation parameters. Standard deviation values for individual blocks are available in Annex 8: Mission Summary Reports.

#### 3.5 LiDAR Data Quality Checking

The boundary of the processed LiDAR data on top of a SAR Elevation Data over Caramay Floodplain is shown in Figure 11. The map shows gaps in the LiDAR coverage that are attributed to cloud coverage.



Figure 11. Boundary of the processed LiDAR data over Caramay Floodplain

The total area covered by the Caramay missions is 149.84 sq.km that is comprised of five (5) flight acquisitions grouped and merged into two (2) blocks as shown in Table 10.

| LiDAR Blocks              | Flight Numbers | Area (sq. km) |  |
|---------------------------|----------------|---------------|--|
|                           | 3505G          |               |  |
| Palawan_reflights_Blk42eA | 3507G          | 106.01        |  |
|                           | 3513G          |               |  |
|                           | 3517G          | 42.02         |  |
| Palawan_reflights_Blk42eB | 3545G          | 43.83         |  |
| TOTAL                     |                | 149.84 sq.km  |  |

| Table 10. Lis | st of LiDAR | blocks for | Caramay | floodplain. |
|---------------|-------------|------------|---------|-------------|
|               |             |            |         |             |

The overlap data for the merged LiDAR blocks, showing the number of channels that pass through a particular location is shown in Figure 12. Since the Gemini system employs one channel, we would expect an average value of 1 (blue) for areas where there is limited overlap, and a value of 2 (yellow) or more (red) for areas with three or more overlapping flight lines.



Figure 12. Image of data overlap for Caramay Floodplain.

The overlap statistics per block for the Caramay floodplain can be found in Annex 8. One pixel corresponds to 25.0 square meters on the ground. For this area, the minimum and maximum percent overlaps are 36.93% and 70.34% respectively, which passed the 25% requirement.

The pulse density map for the merged LiDAR data, with the red parts showing the portions of the data that satisfy the 2 points per square meter criterion is shown in Figure 13. It was determined that all LiDAR data for Caramay floodplain satisfy the point density requirement, and the average density for the entire survey area is 4.82 points per square meter.



Figure 13. Pulse density map of merged LiDAR data for Caramay Floodplain.

The elevation difference between overlaps of adjacent flight lines is shown in Figure 14. The default color range is from blue to red, where bright blue areas correspond to portions where elevations of a previous flight line, identified by its acquisition time, are higher by more than 0.20m relative to elevations of its adjacent flight line. Bright red areas indicate portions where elevations of a previous flight line are lower by more than 0.20m relative to elevations of its adjacent flight line. Areas with bright red or bright blue need to be investigated further using Quick Terrain Modeler software.



Figure 14. Elevation difference map between flight lines for Caramay Floodplain.

A screen capture of the processed LAS data from a Caramay flight 3507G loaded in QT Modeler is shown in Figure 15. The upper left image shows the elevations of the points from two overlapping flight strips traversed by the profile, illustrated by a dashed red line. The x-axis corresponds to the length of the profile. It is evident that there are differences in elevation, but the differences do not exceed the 20-centimeter mark. This profiling was repeated until the quality of the LiDAR data becomes satisfactory. No reprocessing was done for this LiDAR dataset.



Figure 15. Quality checking for Caramay flight 3507G using the Profile Tool of QT Modeler.

#### 3.6 LiDAR Point Cloud Classification and Rasterization

| Pertinent Class   | Total Number of Points |
|-------------------|------------------------|
| Ground            | 38,622,821             |
| Low Vegetation    | 290,137,517            |
| Medium Vegetation | 206,214,236            |
| High Vegetation   | 352,934,713            |
| Building          | 5,722,416              |

Table 11. Caramay classification results in TerraScan.

The tile system that TerraScan employed for the LiDAR data and the final classification image for a block in Caramay floodplain is shown in Figure 16. A total of 226 1km by 1km tiles were produced. The number of points classified to the pertinent categories is illustrated in Table 11. The point cloud has a maximum and minimum height of 514.64 meters and 50.38 meters respectively.



Figure 16. Tiles for Caramay Floodplain (a) and classification results (b) in TerraScan.

An isometric view of an area before and after running the classification routines is shown in Figure 17. The ground points are in orange, the vegetation is in different shades of green, and the buildings are in cyan. It can be seen that residential structures adjacent or even below canopy are classified correctly, due to the density of the LiDAR data.



Figure 17. Point cloud before (a) and after (b) classification.

The production of last return (V\_ASCII) and the secondary (T\_ASCII) DTM, first (S\_ASCII) and last (D\_ASCII) return DSM of the area in top view display are shown in Figure 18. It shows that DTMs are the representation of the bare earth while on the DSMs, all features are present such as buildings and vegetation.



Figure 18. The production of last return DSM (a) and DTM (b), first return DSM (c) and secondary DTM (d) in some portion of Caramay floodplain.

### 3.7 LiDAR Image Processing and Orthophotograph Rectification

There are no available orthophotographs for the Caramay floodplain.

#### 3.8 DEM Editing and Hydro-Correction

Two (2) mission blocks were processed for Caramay flood plain. These blocks are composed of Palawan\_ reflights blocks with a total area of 149.84 square kilometers. Table 12 shows the name and corresponding area of each block in square kilometers.

| LiDAR Blocks              | Area (sq.km) |
|---------------------------|--------------|
| Palawan_reflights_Blk42eA | 106.01       |
| Palawan_reflights_Blk42eB | 43.83        |
| TOTAL                     | 149.84 sq.km |

| Table 12. LiDAR blocks with its corresponding area |
|--|
|--|

Portions of DTM before and after manual editing are shown in Figure 19. The bridge (Figure 19a) is also considered to be an impedance to the flow of water along the river and has to be removed (Figure 19b) in order to hydrologically correct the river. The paddy field (Figure 19c) has been misclassified and removed during classification process and has to be retrieved to complete the surface (Figure 19d) to allow the correct flow of water.



Figure 19. Portions in the DTM of Caramay floodplain – a bridge before (a) and after (b) manual editing; a paddy field before (c) and after (d) data retrieval.

#### 3.9 Mosaicking of Blocks

Palawan\_Blk42Aa was used as the reference block at the start of mosaicking because it was the first block mosaicked to the larger DTM of West Coast Palawan. Upon inspection of the blocks mosaicked for the Caramay floodplain, it was concluded that the elevation of both blocks needed adjustment. Table 13 shows the shift values applied to each LiDAR block during mosaicking.

Mosaicked LiDAR DTM for Caramay floodplain is shown in Figure 20. The entire Caramay flood plain is 99.18% covered by LiDAR data while portions with no LiDAR data were patched with the available IFSAR data.

| Mission Plasks            | Shift Values (meters) |      |        |  |
|---------------------------|-----------------------|------|--------|--|
|                           | х                     | У    | z      |  |
| Palawan_reflights_Blk42eA | 0.54                  | 0.75 | -12.81 |  |
| Palawan_reflights_Blk42eB | 0.54                  | 0.75 | -0.53  |  |

| rubie 19. office ( urdeo of each Eibrine bioen of Ouruning) i lood plant. |
|---|
|---|



Figure 20. Map of Processed LiDAR Data for Caramay Floodplain.

#### 3.10 Calibration and Validation of Mosaicked LiDAR Digital Elevation Model

The extent of the validation survey done by the Data Validation and Bathymetry Component (DVBC) in Caramay to collect points with which the LiDAR dataset is validated is shown in Figure 21. A total of 990 survey points were used for calibration and validation of Caramay LiDAR data. Random selection of 80% of the survey points, resulting to 793 points, was used for calibration.

A good correlation between the uncalibrated mosaicked LiDAR elevation values and the ground survey elevation values is shown in Figure 22. Statistical values were computed from extracted LiDAR values using the selected points to assess the quality of data and obtain the value for vertical adjustment. The computed height difference between the LiDAR DTM and calibration elevation values is 11.18 meters with a standard deviation of 0.19 meters. Calibration of Caramay LiDAR data was done by adding the height difference value, 11.18 meters, to Caramay mosaicked LiDAR data. Table 14 shows the statistical values of the compared elevation values between LiDAR data and calibration data.



Figure 21. Map of Caramay Floodplain with validation survey points in green.


Figure 22. Correlation plot between calibration survey points and LiDAR data.

| Calibration Statistical Measures | Value (meters) |
|----------------------------------|----------------|
| Height Difference                | 11.18          |
| Standard Deviation               | 0.19           |
| Average                          | 11.17          |
| Minimum                          | 10.80          |
| Maximum                          | 11.55          |

Table 14. Calibration Statistical Measures.

The remaining 20% of the total survey points, resulting to 197, were used for the validation of calibrated Caramay DTM. A good correlation between the calibrated mosaicked LiDAR elevation values and the ground survey elevation, which reflects the quality of the LiDAR DTM is shown in Figure 23. The computed RMSE between the calibrated LiDAR DTM and validation elevation values is 11.16 meters with a standard deviation of 0.12 meters, as shown in Table 15.



Figure 23. Correlation plot between validation survey points and LiDAR data.

| Validation Statistical Measures | Value (meters) |
|---------------------------------|----------------|
| RMSE                            | 11.16          |
| Standard Deviation              | 0.12           |
| Average                         | 11.16          |
| Minimum                         | 10.92          |
| Maximum                         | 11.41          |

Table 15. Validation Statistical Measures.

# 3.11 Integration of Bathymetric Data into the LiDAR Digital Terrain Model

For bathymetric data integration, centerline and cross section were available for Caramay with a total of 10,321 survey points. The resulting raster surface produced was done by Inverse Distance Weighted (IDW) interpolation method. After burning the bathymetric data to the calibrated DTM, assessment of the interpolated surface is represented by the computed RMSE value of 0.29 meters. The extent of the bathymetric survey done by the Data Validation and Bathymetry Component (DVBC) in Caramay integrated with the processed LiDAR DEM is shown in Figure 24.



Figure 24. Map of Caramay Floodplain with bathymetric survey points shown in blue.

# 3.12 Feature Extraction

The features salient in flood hazard exposure analysis include buildings, road networks, bridges and water bodies within the floodplain area with 200 m buffer zone. Mosaicked LiDAR DEM with 1 m resolution was used to delineate footprints of building features, which consist of residential buildings, government offices, medical facilities, religious institutions, and commercial establishments, among others. Road networks comprise of main thoroughfares such as highways and municipal and barangay roads essential for routing of disaster response efforts. These features are represented by a network of road centerlines.

### 3.12.1 Quality Checking of Digitized Features' Boundary

Caramay floodplain, including its 200 m buffer, has a total area of 17.72 sq km. For this area, a total of 5.0 sq km, corresponding to a total of 251 building features, are considered for QC. Figure 25 shows the QC blocks for Caramay floodplain.



Figure 25. QC blocks for Caramay building features.

Quality checking of Caramay building features resulted in the ratings shown in Table 16.

Table 16. Quality Checking Ratings for Caramay Building Features.

| FLOODPLAIN | COMPLETENESS | CORRECTNESS | QUALITY | REMARKS |
|------------|--------------|-------------|---------|---------|
| Caramay    | 96.90        | 99.60       | 93.63   | PASSED  |

### 3.12.2 Height Extraction

Height extraction was done for 5,690 building features in Caramay floodplain. Of these building features, none was filtered out after height extraction, resulting to 5,690 buildings with height attributes. The lowest building height is at 2.00 m, while the highest building is at 8.74 m.

### 3.12.3 Feature Attribution

A field team was deployed to the floodplain areas to gather attribute data for the features. Point features in .gpx format were generated from the feature shapefiles. These were loaded into OsmAnd, a mobile mapping application that uses OpenStreetMap (OSM) data as base map. Attributes of feature points of interest (POIs) such as government institutions, social service facilities, agro-industrial facilities, commercial buildings, and transportation and utility offices were recorded. These attributes include building types and names. Names and types of roads were also noted. For water bodies and bridges, only the names were recorded.

Table 17 summarizes the number of building features per type. On the other hand, Table 18 shows the total length of each road type, while Table 19 shows the number of water features extracted per type.

| Facility Type                           | No. of Features |
|---|-----------------|
| Residential                             | 758             |
| School                                  | 14              |
| Market                                  | 1               |
| Agricultural/Agro-Industrial Facilities | 0               |
| Medical Institutions                    | 1               |
| Barangay Hall                           | 0               |
| Military Institution                    | 0               |
| Sports Center/Gymnasium/Covered Court   | 9               |
| Telecommunication Facilities            | 0               |
| Transport Terminal                      | 0               |
| Warehouse                               | 0               |
| Power Plant/Substation                  | 2               |
| NGO/CSO Offices                         | 0               |
| Police Station                          | 0               |
| Water Supply/Sewerage                   | 6               |
| Religious Institutions                  | 8               |
| Bank                                    | 0               |
| Factory                                 | 0               |
| Gas Station                             | 0               |
| Fire Station                            | 0               |
| Other Government Offices                | 10              |
| Other Commercial Establishments         | 0               |
| Total                                   | 807             |

Table 17. Building Features Extracted for Caramay Floodplain.

|            |                  | Road Netwo             | ork Length (kn     | n)               |        |       |
|------------|------------------|------------------------|--------------------|------------------|--------|-------|
| Floodplain | Barangay<br>Road | City/Municipal<br>Road | Provincial<br>Road | National<br>Road | Others | Total |
| Caramay    | 14.00            | 0.00                   | 0.00               | 6.20             | 0.00   | 20.20 |

### Table 18. Total Length of Extracted Roads for Caramay Floodplain.

Table 19. Number of Extracted Water Bodies for Caramay Floodplain.

| Floodalain |                       | Water Bo    | ody Type |     |          | Total |
|------------|-----------------------|-------------|----------|-----|----------|-------|
| riooupiain | <b>Rivers/Streams</b> | Lakes/Ponds | Sea      | Dam | Fish Pen | IOtal |
| Caramay    | 1                     | 0           | 1        | 0   | 0        | 2     |

A total of 44 bridges and culverts over small channels that are part of the river network were also extracted for the floodplain.

### 3.12.4 Final Quality Checking of Extracted Features

All extracted ground features were completely given the required attributes. All these output features comprise the flood hazard exposure database for the floodplain. This completes the feature extraction phase of the project.

Figure 26 shows the Digital Surface Model (DSM) of Caramay floodplain overlaid with its ground features.



Figure 26. Extracted features for Caramay Floodplain.

# CHAPTER 4: LIDAR VALIDATION SURVEY AND MEASUREMENTS OF CARAMAY RIVER BASIN

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The methods applied in this Chapter were based on the DREAM methods manual (Balicanta, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

# 4.1 Summary of Activities

The Data Validation and Bathymetry Component (DVBC) conducted a field survey in Caramay River on November 15 – 29, 2016 with the following scope of work: reconnaissance; control survey; cross-section and as-built surveys at Caramay Bridge in Brgy. Caramay, Municipality of Roxas; validation points acquisition of about 14 km covering the Barangays: Tagumpay, Rizal, Salvacion, Caramay, and Nicanor Zabala in the Municipality of Roxas; and bathymetric survey from its upstream in Brgy. Caramay, in the Municipality of Roxas, to the mouth of the river in the same barangay, with an approximate length of 5.931 km using Trimble<sup>®</sup> SPS 985 GNSS PPK survey technique. The entire survey extent is illustrated in Figure 27.



Figure 27. Caramay River Basin Survey Extent

# 4.2 Control Survey

A GNSS network was established for a previous PHIL-LIDAR 1 DVBC fieldwork in Babuyan River on November 6, 2015 occupying the control points PLW-7, a 2<sup>nd</sup> order GCP in Brgy. Maningning, Puerto Princesa City, Palawan; and PL-188, a 1<sup>st</sup> order Benchmark in Brgy. Langogan, Puerto Princesa City, Palawan.

The GNSS network used for Caramay River Basin is composed of four (4) loops established on November 16, 2016, occupying the reference points: PL-188, a 1<sup>st</sup> order BM in Brgy. Langogan, Puerto Princesa City; and UP-BAB, a UP established control point in Brgy. Babuyan, Puerto Princesa City in Palawan, both fixed from Babuyan Survey.

A control point was established namely UP-BRN located near Port Barton in Brgy. Port Barton, Municipality of San Vicente, Palawan. A NAMRIA established control point namely, PLW-200, in Brgy. 1 Poblacion, Municipality of Roxas, and PLW-3018, in Brgy. Caramay, Municipality of Roxas, Palawan; were also occupied to use as markers for the survey.

The summary of reference and control points and its location is summarized in Table 20 while the GNSS network established is illustrated in Figure 28.



Figure 28. GNSS Network covering Caramay River

Table 20. List of reference and control points used during the survey in Caramay River (Source: NAMRIA, UP-TCAGP)

|               |                   |                 | g                     | ographic Coordinates (WO | 3S 84)            |                  |
|---------------|-------------------|-----------------|-----------------------|--------------------------|-------------------|------------------|
| Control Point | Order of Accuracy | Latitude        | Longitude             | Ellipsoidal Height (m)   | MSL Elevation (m) | Date Established |
|               |                   | Cor             | ntrol Survey on Noven | nber 16, 2016            |                   |                  |
| PL-188        | Fixed             | 10°01′44.89299″ | 119°07'24.55685"      | 57.865                   | 6.467             | 11-06-15         |
| UP-BAB        | Fixed             | 09°59′43.61060″ | 118°53'35.10633"      | 57.562                   | 6.906             | 11-06-15         |
| PLW-200       | Used as marker    | I               | I                     |                          | ı                 | 11-16-16         |
| PLW-3018      | Used as marker    | I               | I                     |                          | ı                 | 11-16-16         |
| UP-BRN        | UP established    | I               | I                     |                          | I                 | 11-16-16         |
|               |                   | Co              | ntrol Survey on Nover | nber 6, 2015             |                   |                  |
| PLW-7         | 2nd Order, GCP    | 09°44'25.33347" | 118°44'25.60607"      | 87.116                   | 36.677            | 11-06-15         |
| PL-188        | 1st Order, BM     | 10°01′44.89299″ | 119°07'24.55685"      | 59.285                   | 6.467             | 11-06-15         |
|               |                   |                 |                       |                          |                   |                  |

The GNSS set-ups on recovered reference points and established control points in Caramay River are shown in Figure 29 to Figure 34.



Figure 29. GNSS receiver setup, Trimble<sup>\*</sup> SPS 985, at PL-188, located at the approach of Langogan Bridge in Brgy. Langogan, Puerto Princesa City, Palawan



Figure 30. GNSS base set up, Trimble<sup>\*</sup> SPS 985, at UP-BAB, located at the approach of Babuyan Bridge in Brgy. Babuyan, Puerto Princesa City, Palawan



Figure 31. GNSS receiver setup, Trimble<sup>®</sup> SPS 985 at PLW-200, located along the shoreline in Brgy. 1 Poblacion, Municipality of Roxas, Palawan



Figure 32. GNSS receiver setup, Trimble<sup>\*</sup> SPS 882, at PLW-3018, located along Puerto Princesa North Road in Brgy. Caramay, Municipality of Roxas, Palawan



Figure 33. GNSS receiver setup, Trimble<sup>®</sup> SPS 852, at UP-BRN, located near Port Barton in Brgy. Port Barton, Municipality of San Vicente, Palawan



Figure 34. GNSS receiver setup, Trimble<sup>®</sup> SPS 852, at PLW-7, located at the top of a concrete water tank inside the Water District Compound in Brgy. Maningning, Puerto Princesa City, Palawan

# 4.3 Baseline Processing

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GNSS Baselines were processed simultaneously in TBC by observing that all baselines have fixed solutions with horizontal and vertical precisions within +/- 20 cm and +/- 10 cm requirement, respectively. In case where one or more baselines did not meet all of these criteria, masking is performed. Masking is done by removing/masking portions of these baseline data using the same processing software. It is repeatedly processed until all baseline requirements are met. If the reiteration yields out of the required accuracy, resurvey is initiated. Baseline processing result of control points in Caramay River Basin is summarized in Table 21 generated by TBC software.

| Table 21. Baseline Processing Report for Caramay R | River Static Survey (Source: NAMRIA, UP-TCAGP) |
|--|--|
|--|--|

| Observation                 | Date of<br>Observation | Solution<br>Type | H.Prec.<br>(Meter) | V.Prec.<br>(Meter) | Geodetic<br>Az. | Ellipsoid<br>Dist.<br>(Meter) | Height<br>(Meter) |
|-----------------------------|------------------------|------------------|--------------------|--------------------|-----------------|-------------------------------|-------------------|
| UP-BAB<br>PL-188 (B6)       | PL-188                 | UP-BAB           | Fixed              | 0.004              | 0.022           | 261°37'42"                    | 25533.641         |
| PLW-3018<br>PL-188<br>(B3)  | PL-188                 | PLW-<br>3018     | Fixed              | 0.003              | 0.012           | 33°39'39"                     | 19973.003         |
| UP-BAB<br>PLW-200<br>(B5)   | UP-BAB                 | PLW-200          | Fixed              | 0.009              | 0.036           | 54°21'18"                     | 60909.606         |
| UP-BAB<br>UP-BRN (B7)       | UP-BAB                 | UP-BRN           | Fixed              | 0.011              | 0.040           | 40°06'28"                     | 52687.150         |
| UP-BAB<br>PLW-3018<br>(B4)  | UP-BAB                 | PLW-<br>3018     | Fixed              | 0.004              | 0.019           | 60°42'58"                     | 41638.975         |
| PLW-3018<br>PLW-200<br>(B2) | PLW-3018               | PLW-200          | Fixed              | 0.003              | 0.014           | 41°07'13"                     | 20064.565         |
| PLW-3018<br>UP-BRN<br>(B8)  | PLW-3018               | UP-BRN           | Fixed              | 0.004              | 0.028           | 353°15'43"                    | 20070.679         |
| PLW-200<br>UP-BRN<br>(B9)   | PLW-200                | UP-BRN           | Fixed              | 0.004              | 0.030           | 287°13'56"                    | 16279.087         |
| PL-188<br>PLW-200<br>(B1)   | PL-188                 | PLW-200          | Fixed              | 0.003              | 0.015           | 37°23′24″                     | 39953.172         |
| PL-188<br>UP-BRN<br>(B10)   | PL-188                 | UP-BRN           | Fixed              | 0.005              | 0.053           | 13°24'03"                     | 37578.719         |

As shown Table 21 a total of ten (10) baselines were processed with coordinate and elevation values of PL-188 and UP-BAB, both fixed from previous PHIL-LIDAR1 survey in Babuyan River; held fixed. All of them passed the required accuracy.

# 4.4 Network Adjustment

After the baseline processing procedure, network adjustment is performed using TBC. Looking at the Adjusted Grid Coordinates table of the TBC generated Network Adjustment Report, it is observed that the square root of the sum of the squares of x and y must be less than 20 cm and z less than 10 cm or in equation from:

$$\sqrt{((x_e)^2 + (y_e)^2)}\sqrt{((x_e)^2 + (y_e)^2)}$$
 <20cm and  $z_e < 10 \text{ cm } z_e < 10 \text{ cm}$ 

Where:

 $x_e$  is the Easting Error,  $y_e$  is the Northing Error, and  $z_e$  is the Elevation Error

for each control point. See the Network Adjustment Report shown in Table 22 to Table 25 for complete details.

The five (5) control points, PL-188, PLW-200, PLW-3018, UP-BAB, and UP-BRN were occupied and observed simultaneously to form a GNSS loop. Coordinates and elevation values of PL-188 and UP-BAB were held fixed during the processing of the control points as presented in Table 22. Through these reference points, the coordinates and elevation of the unknown control points will be computed.

| Point ID                 | Туре | East σ<br>(Meter) | North σ<br>(Meter) | Height σ<br>(Meter) | Elevation σ<br>(Meter) |  |  |
|--------------------------|------|-------------------|--------------------|---------------------|------------------------|--|--|
| PL-188                   | Grid | Fixed             | Fixed              |                     | Fixed                  |  |  |
| UP-BAB                   | Grid | Fixed             | Fixed              |                     | Fixed                  |  |  |
| Fixed = 0.000001 (Meter) |      |                   |                    |                     |                        |  |  |

The list of adjusted grid coordinates, i.e. Northing, Easting, Elevation and computed standard errors of the control points in the network is indicated in Table 23. All fixed control points have no values for grid and elevation errors.

### Table 23. Adjusted Grid Coordinates

| Point ID | Easting<br>(Meter) | Easting<br>Error<br>(Meter) | Northing<br>(Meter) | Northing<br>Error<br>(Meter) | Elevation<br>(Meter) | Elevation<br>Error<br>(Meter) | Constraint |
|----------|--------------------|-----------------------------|---------------------|------------------------------|----------------------|-------------------------------|------------|
| PL-188   | 74882.789          | ?                           | 1111141.315         | ?                            | 6.467                | ?                             | ENe        |
| PLW-200  | 99564.013          | 0.013                       | 1142646.180         | 0.012                        | 2.161                | 0.041                         |            |
| PLW-3018 | 86170.148          | 0.008                       | 1127662.105         | 0.008                        | 17.691               | 0.036                         |            |
| UP-BAB   | 49529.234          | ?                           | 1107714.958         | ?                            | 6.906                | ?                             | ENe        |
| UP-BRN   | 84046.211          | 0.012                       | 1147655.023         | 0.012                        | 36.026               | 0.065                         |            |

With the mentioned equation  $\sqrt{((x_e)^2 + (y_e)^2)} < 20 cm \sqrt{((x_e)^2 + (y_e)^2)} < 20 cm$  for the horizontal and  $z_e < 10 cm z_e < 10 cm$  for the vertical; the computation for the accuracy for:

| PL-1 | 188                 | _    | Fixed                              |  |  |  |
|------|---------------------|------|------------------------------------|--|--|--|
|      |                     | =    | Fixed                              |  |  |  |
|      | vertical accuracy   | =    | Fixed                              |  |  |  |
| UP-  | BAB                 |      |                                    |  |  |  |
|      | horizontal accuracy | =    | Fixed                              |  |  |  |
|      | vertical accuracy   | =    | Fixed                              |  |  |  |
| ЫΜ   | /-200               |      |                                    |  |  |  |
|      | horizontal accuracy | =    | $\sqrt{((1 \ 3)^2 + (1 \ 2)^2)^2}$ |  |  |  |
|      | =                   | v (1 | $69 + 1 \Lambda 1$                 |  |  |  |
|      | _                   | 1 7  | 7 < 20  cm                         |  |  |  |
|      |                     | 1.77 |                                    |  |  |  |
|      | vertical accuracy   | =    | 4.1 < 10 cm                        |  |  |  |
| PLW  | /-3018              |      |                                    |  |  |  |
|      | horizontal accuracy | =    | $V((0.8)^2 + (0.8)^2)$             |  |  |  |
|      |                     | =    | √ (0.64 + 0.64)                    |  |  |  |
|      |                     | =    | 1.13 < 20 cm                       |  |  |  |
|      | vertical accuracy   | =    | 3.6 < 10 cm                        |  |  |  |
| UP-  | BRN                 |      |                                    |  |  |  |
|      | horizontal accuracy | =    | $\sqrt{((1.2)^2 + (1.2)^2)}$       |  |  |  |
|      |                     | =    | √ (1.44 + 1.44)                    |  |  |  |
|      |                     | =    | 1.70 < 20  cm                      |  |  |  |
|      | vertical accuracy   | _    | 65 < 10  cm                        |  |  |  |
|      | vertical accuracy   | _    | 0.0 < 10 011                       |  |  |  |

Following the given formula, the horizontal and vertical accuracy result of the two (2) occupied control points are within the required precision.

| Point ID | Latitude         | Longitude         | Ellipsoid<br>Height<br>(Meter) | Height<br>Error<br>(Meter) | Constraint |
|----------|------------------|-------------------|--------------------------------|----------------------------|------------|
| PL-188   | N10°01′44.89299″ | E119°07'24.55685" | 57.865                         | ?                          | ENe        |
| PLW-200  | N10°18′57.78651″ | E119°20'41.94774" | 53.650                         | 0.041                      |            |
| PLW-3018 | N10°10′45.91002″ | E119°13'28.25701" | 69.163                         | 0.036                      |            |
| UP-BAB   | N9°59′43.61060″  | E118°53'35.10633" | 57.562                         | ?                          | ENe        |
| UP-BRN   | N10°21'34.63416" | E119°12'10.84685" | 87.058                         | 0.065                      |            |

Table 24. Adjusted Geodetic Coordinates

The corresponding geodetic coordinates of the observed points are within the required accuracy as shown in Table 25. Based on the result of the computation, the accuracy condition is satisfied; hence, the required accuracy for the program was met.

The summary of reference and control points used is indicated in Table 25.

Table 25. Reference and control points and its location (Source: NAMRIA, UP-TCAGP)

| UTM ZONE 51 N                   | BM Ortho<br>(m)           |                          | 6.467            | 906.9            | 2.161             | 17.691            | 36.026           |                          | 6.467            | 35.257            |           |           |
|---------------------------------|---------------------------|--------------------------|------------------|------------------|-------------------|-------------------|------------------|--------------------------|------------------|-------------------|-----------|-----------|
|                                 | Easting (m)               |                          |                  |                  | 74882.789         | 49529.234         | 99564.013        | 86170.148                | 84046.211        |                   | 74882.789 | 32397.249 |
|                                 | Northing (m)              |                          | 1111141.315      | 1107714.958      | 1142646.18        | 1127662.105       | 1147655.023      |                          | 1111141.315      | 1079651.883       |           |           |
| Geographic Coordinates (WGS 84) | Ellipsoidal Height<br>(m) | er 16, 2016              | 57.865           | 57.562           | 53.65             | 69.163            | 87.058           | er 6, 2015               | 59.285           | 87.116            |           |           |
|                                 | Longitude                 | ontrol Survey on Novembe | 119d07'24.55685" | 118d53'35.10633" | 119d20'41.94774"  | 119d13'28.25701"  | 119d12'10.84685" | Control Survey on Novemb | 119d07'24.55686" | 118d44'25.60607"  |           |           |
|                                 | Latitude                  | 0                        | 10d01'44.89299"  | 9d59'43.61060"   | 10d18′57.78651″   | 10d10'45.91002"   | 10d21'34.63416"  | 0                        | 10d01'44.89298"  | 9d44'25.33347"    |           |           |
| Order of                        | Accuracy                  |                          | Fixed            | Fixed            | Used as<br>marker | Used as<br>marker | UP established   |                          | 1st Order, BM    | 2nd Order,<br>GCP |           |           |
| Control Point                   |                           |                          | PL-188           | UP-BAB           | PLW-200           | PLW-3018          | UP-BRN           |                          | PL-188           | PLW-7             |           |           |

# 4.5 Cross-section and Bridge As-Built Survey, and Water Level Marking

Cross-section and as-built surveys were conducted on November 18, 2016 at the downstream side of Caramay bridge in Brgy. Caramay, Municipality of Roxas, Palawan as shown in Figure 35. A survey grade GNSS receiver Trimble<sup>®</sup> SPS 985 in PPK survey technique was utilized for this survey as shown in Figure 36.



Figure 35. Caramay Bridge facing downstream



Figure 36. As-built survey of Caramay Bridge

The cross-sectional line of Caramay Bridge is about 172.856 m with ninety-four (94) cross-sectional points, using the control point PLW-3018 as the GNSS base station. The location map, cross-section diagram, and the bridge data form is shown in Figure 37 to Figure 39.



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Figure 38. Caramay Bridge cross-section diagram



| 30 m | 10 022   |               |
|------|----------|---------------|
|      | 10.022 m |               |
| 50 m | 10.112 m |               |
| 01 m | 10.098 m |               |
| 41 m | 10.039 m |               |
|      | 41 m     | 41 m 10.039 m |

NOTE: Use the center of the pier as reference to its station

Figure 39. Bridge as-built form of Caramay Bridge

Water surface elevation of Caramay River was determined by a survey grade GNSS receiver Trimble<sup>®</sup> SPS 985 in PPK survey technique on November 18, 2016 at 10:39 AM at Caramay Bridge with a value of -0.169 m in MSL as shown in Figure 38. This was translated into marking on the bridge's abutment as shown in Figure 40. The marking will serve as reference for flow data gathering and depth gauge deployment of the partner HEI responsible for Caramay River, the University of the Philippines Los Baños.

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)



Figure 40. Water-level marking at Caramay Bridge

# 4.6 Validation Points Acquisition Survey

Validation points acquisition survey was conducted on November 18, 2016 using a survey-grade GNSS Rover receiver, Trimble<sup>®</sup> SPS 985, mounted in front of a vehicle as shown in Figure 41. It was secured with a nylon rope to ensure that it was horizontally and vertically balanced. The antenna height was 2.23 m and measured from the ground up to the bottom of notch of the GNSS Rover receiver. The PPK technique utilized for the conduct of the survey was set to continuous topo mode with PLW-3018 occupied as the GNSS base station in the conduct of the survey.



Figure 41. Validation points acquisition survey set-up for Caramay River

The survey started in Brgy. Tagumpay, Municipality of Roxas going south along national highway covering barangays Caramay, Rizal, Salvacion, and ended in Brgy. Nicanor Zabala, Municipality of Roxas, Plawan. A total of 1,635 points with approximate length of 14 km using PLW-3018 as GNSS base station for the entire extent validation points acquisition survey as illustrated in the map in Figure 42.



Figure 42. Validation point acquisition survey of Caramay River Basin

# 4.7 Bathymetric Survey

Manual Bathymetric survey was executed on November 18 and 20, 2016 using Trimble<sup>®</sup> SPS 985 in GNSS PPK survey technique in continuous topo mode as illustrated in Figure 43. It started in Brgy. Caramay, Municipality of Roxas with coordinates 10°10′28.56384″N, 119°11′50.39948″E, traversed down the river by foot and ended at the mouth of the river in the same barangay with coordinates 10°10′46.27159″N, 119°14′02.08970″E. The control points PLW-3018 was used as GNSS base stations all throughout the entire survey.



Figure 43. Manual Bathymetric survey using a Trimble\* SPS 985 in GNSS PPK survey technique in Caramay River

The bathymetric survey for Caramay River gathered a total of 10,670 points covering 5.931 km of the river traversing Brgy. Caramay, Municipality of Roxas, Palawan (Figure 44).



Figure 44. Bathymetric survey of Caramay River

A CAD drawing was also produced to illustrate the riverbed profile of Caramay River. As shown in Figure 45, the highest and lowest elevation has a 11-m difference. The highest elevation observed was 8.664 m above MSL located at the upstream part of the river; while the lowest was –2.465 m below MSL located a kilometer from the river's mouth.



# **Caramay Riverbed Profile**

Figure 45. Caramay riverbed profile

# **CHAPTER 5: FLOOD MODELING AND MAPPING**

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The methods applied in this Chapter were based on the DREAM methods manual (Lagmay, et al., 2014) and further enhanced and updated in Paringit, et al. (2017).

# 5.1 Data used in Hydrologic Modeling

No gathered rainfall data for Caramay river basin. The HMS model is not calibrated. The values generated HMS model are by default.

# **5.2 RIDF Station**

The Philippines Atmospheric Geophysical and Astronomical Services Administration (PAGASA) computed Rainfall Intensity Duration Frequency (RIDF) values for the Puerto Princesa Rain Gauge. The RIDF rainfall amount for 24 hours was converted to a synthetic storm by interpolating and re-arranging the values in such a way a certain peak value will be attained at a certain time. This station chosen based on its proximity to the Caramay watershed. The extreme values for this watershed were computed based on a 58-year record, with the computed extreme values shown in Table 26.

| COMPUTED EXTREME VALUES (in mm) OF PRECIPITATION |         |         |         |      |       |       |       |        |        |  |
|--|---------|---------|---------|------|-------|-------|-------|--------|--------|--|
| T (yrs)  | 10 mins | 20 mins | 30 mins | 1 hr | 2 hrs | 3 hrs | 6 hrs | 12 hrs | 24 hrs |  |
| 2  | 14.8    | 22      | 27.3    | 36.2 | 49.8  | 58.8  | 75.1  | 88     | 104.1  |  |
| 5  | 21.3    | 31.9    | 39.7    | 52.3 | 73    | 86.9  | 112.8 | 135.4  | 156.4  |  |
| 10   | 25.6    | 38.5    | 48      | 63   | 88.4  | 105.5 | 137.8 | 166.8  | 191.1  |  |
| 15   | 28.1    | 42.2    | 52.6    | 69   | 97    | 116   | 151.9 | 184.5  | 210.6  |  |
| 20   | 29.8    | 44.7    | 55.9    | 73.3 | 103.1 | 123.4 | 161.7 | 196.8  | 224.3  |  |
| 25   | 31.1    | 46.7    | 58.4    | 76.5 | 107.8 | 129.1 | 169.3 | 206.4  | 234.9  |  |
| 50   | 35.2    | 52.9    | 66.1    | 86.5 | 122.2 | 146.5 | 192.7 | 235.8  | 267.3  |  |
| 100  | 39.2    | 59      | 73.7    | 96.4 | 136.5 | 163.8 | 216   | 265    | 299.6  |  |

Table 26. RIDF values for Puerto Princesa Rain Gauge computed by PAGASA



Figure 46.Location of Puerto Princesa RIDF relative to Caramay River Basin



Figure 47. Synthetic storm generated for a 24-hr period rainfall for various return periods.

# 5.3 HMS Model

The soil dataset was generated before 2004 by the Bureau of Soils and Water Management under the Department of Agriculture (DA-BSWM). The land cover dataset is from the National Mapping and Resource information Authority (NAMRIA). The soil and land cover of the Caramay River Basin are shown in Figure 48 and Figure 49, respectively.



Figure 48. Soil map of Caramay River Basin used for the estimation of the CN parameter. (Source: DA)



Figure 49. Land cover map of Caramay River Basin used for the estimation of the CN and watershed lag parameters of the rainfall-runoff model. (Source: NAMRIA)

For Caramay river basin, five (5) soil classes were identified. The river basin area is largely rough mountainous land, with portions of San Manuel clay loam, Coron clay loam, beach sand, and hydrosol. Moreover, the three (3) land cover types identified were closed canopy, brushland, and built-up area.



Figure 50. Slope map of Caramay River Basin



Figure 51. Stream delineation map of Caramay River Basin

Using SAR-based DEM, the Caramay basin was delineated and further subdivided into subbasins. The model consists of 64 sub basins, 31 reaches, and 30 junctions. The main outlet is labelled as 90. This basin model is illustrated in Figure 52. The basins were identified based on soil and land cover characteristics of the area.



Figure 52. HEC-HMS generated Caramay River Basin Model.

# 5.4 Cross-section Data

Riverbed cross-sections of the watershed are crucial in the HEC-RAS model setup. The cross-section data for the HEC-RAS model was derived using the LiDAR DEM data. It was defined using the Arc GeoRAS tool and was post-processed in ArcGIS.

[PLACEHOLDER FOR FIGURE 53]

Figure 53. River cross-section of Caramay River generated through Arcmap HEC GeoRAS tool
# 5.5 Flo 2D Model

The automated modelling process allows for the creation of a model with boundaries that are almost exactly coincidental with that of the catchment area. As such, they have approximately the same land area and location. The entire area is divided into square grid elements, 10 meter by 10 meter in size. Each element is assigned a unique grid element number which serves as its identifier, then attributed with the parameters required for modelling such as x-and y-coordinate of centroid, names of adjacent grid elements, Manning coefficient of roughness, infiltration, and elevation value. The elements are arranged spatially to form the model, allowing the software to simulate the flow of water across the grid elements and in eight directions (north, south, east, west, northeast, northwest, southeast, southwest).

Based on the elevation and flow direction, it is seen that the water will generally flow from the west of the model to the east, following the main channel. As such, boundary elements in those particular regions of the model are assigned as inflow and outflow elements respectively.



Figure 54. Screenshot of subcatchment with the computational area to be modeled in FLO-2D GDS Pro

The simulation is then run through FLO-2D GDS Pro. This particular model had a computer run time of 62.10889 hours. After the simulation, FLO-2D Mapper Pro is used to transform the simulation results into spatial data that shows flood hazard levels, as well as the extent and inundation of the flood. Assigning the appropriate flood depth and velocity values for Low, Medium, and High creates the following food hazard map. Most of the default values given by FLO-2D Mapper Pro are used, except for those in the Low hazard level. For this particular level, the minimum h (Maximum depth) is set at 0.2 m while the minimum vh (Product of maximum velocity (v) times maximum depth (h)) is set at 0 m<sup>2</sup>/s.

The creation of a flood hazard map from the model also automatically creates a flow depth map depicting the maximum amount of inundation for every grid element. The legend used by default in Flo-2D Mapper is not a good representation of the range of flood inundation values, so a different legend is used for the layout. In this particular model, the inundated parts cover a maximum land area of 42 550 500.00 m<sup>2</sup>.

There is a total of 44 398 597.41 m<sup>3</sup> of water entering the model. Of this amount, 13 786 789.76 m<sup>3</sup> is due to rainfall while 30 611 807.65 m<sup>3</sup> is inflow from other areas outside the model. 3 832 964.25 m<sup>3</sup> of this water is lost to infiltration and interception, while 4 748 953.07 m<sup>3</sup> is stored by the flood plain. The rest, amounting up to 35 816 663.38 m<sup>3</sup>, is outflow.

# 5.6 HEC-HMS Model Values (Uncalibrated)

Enumerated in Table 27 are the range of values of the parameters in the model.

| Hydrologic<br>Element | Calculation<br>Type | Method           | Parameter                  | Range of<br>Values |
|-----------------------|---------------------|------------------|----------------------------|--------------------|
|                       | Loss                |                  | Initial Abstraction (mm)   | 5 - 14             |
| Basin                 | LUSS                | SCS Curve number | Curve Number               | 48 - 73            |
|                       | Tropologia          | Clark Unit       | Time of Concentration (hr) | 0.2 - 2            |
|                       | Iransiorin          | Hydrograph       | Storage Coefficient (hr)   | 0.3 - 4            |

Table 27. Range of calibrated values for Caramay River Basin

Initial abstraction defines the amount of precipitation that must fall before surface runoff. The magnitude of the outflow hydrograph increases as initial abstraction decreases. The range of values from 5 to 14mm means that there is minimal amount of infiltration or rainfall interception by vegetation.

Curve number is the estimate of the precipitation excess of soil cover, land use, and antecedent moisture. The magnitude of the outflow hydrograph increases as curve number increases. The range of 48 to 73 for curve number is slightly lower than the range of advisable values for Philippine watersheds depending on the soil and land cover of the area (M. Horritt, personal communication, 2012).

Time of concentration and storage coefficient are the travel time and index of temporary storage of runoff in a watershed. The range of calibrated values from 0.2 hours to 4 hours determines the reaction time of the model with respect to the rainfall. The peak magnitude of the hydrograph also decreases when these parameters are increased.

# 5.7 River Analysis Model Simulation

The HEC-RAS Flood Model produced a simulated water level at every cross-section for every time step for every flood simulation created. The resulting model will be used in determining the flooded areas within the model. The simulated model will be an integral part in determining real-time flood inundation extent of the river after it has been automated and uploaded on the DREAM website. The sample generated map of Abongan River using the calibrated HMS base flow is shown in Figure 55.



Figure 55. Sample output of Caramay RAS Model

# 5.9 Flood Hazard and Flow Depth Map

The resulting hazard and flow depth maps for 5-, 25-, and 100-year rain return scenarios of the Caramay floodplain are shown in Figure 56 to Figure 61. The floodplain, with an area of 1007.73 sq. km., covers one municipality named Roxas. Table 28 shows the percentage of area affected by flooding per municipality.

| Municipality | Total Area (sq. km) | Area Flooded (sq. km.) | % Flooded |
|--------------|---------------------|------------------------|-----------|
| Roxas        | 1007.73             | 42.48                  | 4.22      |

| Table 28. Municipa | lities affected in   | Caramav F | loodplain |
|--------------------|----------------------|-----------|-----------|
| rubie 20. maineipa | littles affected fif | Curumuy 1 | loodpium  |













# 5.10 Inventory of Areas Exposed to Flooding

Listed below are the barangays affected by the Caramay River Basin, grouped accordingly by municipality. For the said basin, one (1) municipality consisting of 4 barangays are expected to experience flooding when subjected to a 5-year rainfall return period.

For the 5-year return period, 3.38% of the municipality of Roxas with an area of 1007.73 sq. km. will experience flood levels of less 0.20 meters, while 0.23% of the area will experience flood levels of 0.21 to 0.50 meters; 0.23%, 0.22%, 0.11%, and 0.04% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters respectively. Table 29 and Figure 62 depict the areas affected in Roxas in square kilometers by flood depth per barangay.

| Affected Area (sq. km.) | Area of affected barangays in Roxas (in sq. km.) |        |                |           |  |
|-------------------------|--|--------|----------------|-----------|--|
| by flood depth (in m.)  | Caramay  | Magara | Nicanor Zabala | Salvacion |  |
| 0.03-0.20               | 23.85 0.35                                       |        | 3.31           | 6.56      |  |
| 0.21-0.50               | 1.64   | 0.0077 | 0.31           | 0.31      |  |
| 0.51-1.00               | 1.38   | 0.004  | 0.53           | 0.44      |  |
| 1.01-2.00               | 0.96   | 0.006  | 0.85           | 0.41      |  |
| 2.01-5.00               | 0.6  | 0.0065 | 0.46           | 0.065     |  |
| > 5.00                  | 0.39   | 0      | 0.0093         | 0.023     |  |

Table 29. Affected areas in Roxas, Palawan during a 5-Year Rainfall Return Period.



Figure 62. Affected areas in Roxas, Palawan during a 5-Year Rainfall Return Period.

For the 25-year return period, 3.21% of the municipality of Roxas with an area of 1007.73 sq. km. will experience flood levels of less 0.20 meters, while 0.25% of the area will experience flood levels of 0.21 to 0.50 meters; 0.22%, 0.29%, 0.18%, and 0.06% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters respectively. Table 30 and Figure 63 depict the areas affected in Roxas in square kilometers by flood depth per barangay.

| Affected Area (sq. km.) | Area of affected barangays in Roxas (in sq. km.) |            |                |           |  |
|-------------------------|--|------------|----------------|-----------|--|
| by flood depth (in m.)  | Caramay  | Magara     | Nicanor Zabala | Salvacion |  |
| 0.03-0.20               | 22.57  | 22.57 0.35 |                | 6.38      |  |
| 0.21-0.50 1.98          |  | 0.0072     | 0.29           | 0.28      |  |
| 0.51-1.00               | 1.47   | 0.0048     | 0.34           | 0.36      |  |
| 1.01-2.00               | 1.44   | 0.0056     | 0.93           | 0.55      |  |
| 2.01-5.00               | 0.78   | 0.0083     | 0.81           | 0.19      |  |
| > 5.00                  | 0.58   | 0.0009     | 0.027          | 0.031     |  |

Table 30. Affected areas in Roxas, Palawan during a 25-Year Rainfall Return Period.



Figure 63. Affected areas in Roxas, Palawan during a 25-Year Rainfall Return Period.

For the 100-year return period, 3.1% of the municipality of Roxas with an area of 1007.73 sq. km. will experience flood levels of less 0.20 meters, while 0.28% of the area will experience flood levels of 0.21 to 0.50 meters; 0.22%, 0.31%, 0.23%, and 0.08% of the area will experience flood depths of 0.51 to 1 meter, 1.01 to 2 meters, 2.01 to 5 meters, and more than 5 meters respectively. Table 31 and Figure 64 depict the areas affected in Roxas in square kilometers by flood depth per barangay.

| Affected Area (sq. km.) | Area of affected barangays in Roxas (in sq. km.) |        |                |           |  |
|-------------------------|--|--------|----------------|-----------|--|
| by flood depth (in m.)  | Caramay  | Magara | Nicanor Zabala | Salvacion |  |
| 0.03-0.20               | 21.69  | 0.35   | 2.96           | 6.27      |  |
| 0.21-0.50 2.24          |  | 0.0062 | 0.28           | 0.27      |  |
| 0.51-1.00               | 1.56   | 0.0062 | 0.34           | 0.3       |  |
| 1.01-2.00               | 1.68   | 0.0052 | 0.81           | 0.6       |  |
| 2.01-5.00               | 0.96   | 0.01   | 1.05           | 0.32      |  |
| > 5.00                  | 0.69   | 0.0012 | 0.04           | 0.038     |  |

Table 31. Affected areas in Roxas, Palawan during a 100-Year Rainfall Return Period.



Figure 64. Affected areas in Roxas, Palawan during a 100-Year Rainfall Return Period.

Among the barangays in the municipality of Roxas, Caramay is projected to have the highest percentage of area that will experience flood levels of at 2.86%. On the other hand, Salvacion posted the percentage of area that may be affected by flood depths of at 0.77%.

# 5.11 Flood Validation

In order to check and validate the extent of flooding in different river systems, there was a need to perform validation survey work. Field personnel gathered secondary data regarding flood occurrence in the area within the major river system in the Philippines.

From the Flood Depth Maps produced by Phil-LiDAR 1 Program, multiple points representing the different flood depths for different scenarios were identified for validation.

The validation personnel went to the specified points identified in a river basin and gathered data regarding the actual flood level in each location. Data gathering was done through a local DRRM office to obtain maps or situation reports about the past flooding events and through interviews with some residents who have knowledge of or have had experienced flooding in a particular area.

After which, the actual data from the field was compared to the simulated data to assess the accuracy of the Flood Depth Maps produced and to improve on what is needed. The points in the flood map versus its corresponding validation depths are shown in Figure 66.

The flood validation consisted of 49 points randomly selected all over the Caramay floodplain. Comparing it with the flood depth map of the nearest storm event, the map has an RMSE value of 0.67m. Table 32 shows a contingency matrix of the comparison.



Figure 65. Validation points for 25-year Flood Depth Map of Caramay Floodplain



Figure 66. Flood map depth vs. actual flood depth

| Actual             |        | Modeled Flood Depth (m) |           |           |           |        |       |
|--------------------|--------|-------------------------|-----------|-----------|-----------|--------|-------|
| Flood<br>Depth (m) | 0-0.20 | 0.21-0.50               | 0.51-1.00 | 1.01-2.00 | 2.01-5.00 | > 5.00 | Total |
| 0-0.20             | 5      | 1                       | 1         | 0         | 0         | 0      | 7     |
| 0.21-0.50          | 8      | 0                       | 0         | 0         | 0         | 0      | 8     |
| 0.51-1.00          | 7      | 4                       | 2         | 2         | 0         | 0      | 15    |
| 1.01-2.00          | 6      | 6                       | 3         | 4         | 0         | 0      | 19    |
| 2.01-5.00          | 0      | 0                       | 0         | 0         | 0         | 0      | 0     |
| > 5.00             | 0      | 0                       | 0         | 0         | 0         | 0      | 0     |
| Total              | 26     | 11                      | 6         | 6         | 0         | 0      | 49    |

Table 32. Actual flood vs simulated flood depth at different levels in the Caramay River Basin.

The overall accuracy generated by the flood model is estimated at 22.45% with 11 points correctly matching the actual flood depths. In addition, there were 14 points estimated one level above and below the correct flood depths while there were 14 points and 6 points estimated two levels above and below, and three or more levels above and below the correct flood. A total of 4 points were overestimated while a total of 34 points were underestimated in the modelled flood depths of Caramay. Table 33 depicts the summary of the Accuracy Assessment in the Caramay River Basin Survey.

|                | No. of Points | %      |
|----------------|---------------|--------|
| Correct        | 11            | 22.45  |
| Overestimated  | 4             | 8.16   |
| Underestimated | 34            | 69.39  |
| Total          | 49            | 100.00 |

 Table 33. Summary of the Accuracy Assessment in the Caramay River Basin Survey

# REFERENCES

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# ANNEXES

# Annex 1. Optech Technical Specification of the Gemini Sensor



Control Rack

Laptop



| Parameter                       | Specification  |  |
|---------------------------------|--|--|
| Operational envelope (1,2,3,4)  | 150-4000 m AGL, nominal  |  |
| Laser wavelength                | 1064 nm  |  |
| Horizontal accuracy (2)         | 1/5,500 x altitude, (m AGL)  |  |
| Elevation accuracy (2)          | <5-35 cm, 1 σ  |  |
| Effective laser repetition rate | Programmable, 33-167 kHz   |  |
| Position and orientation system | POS AV™ AP50 (OEM);<br>220-channel dual frequency GPS/GNSS/Galileo/L-<br>Band receiver |  |
| Scan width (WOV)                | Programmable, 0-50°  |  |
| Scan frequency (5)              | Programmable, 0-70 Hz (effective)  |  |
| Sensor scan product             | 1000 maximum   |  |
| Beam divergence                 | Dual divergence: 0.25 mrad (1/e) and 0.8 mrad (1/e), nominal                           |  |
| Roll compensation               | Programmable, ±5° (FOV dependent)  |  |

Table A-1.1 Parameters and Specifications of the Gemini Sensor

| Parameter             | Specification   |
|-----------------------|---|
| Range capture         | Up to 4 range measurements, including 1st, 2nd, 3rd, and last returns   |
| Intensity capture     | Up to 4 intensity returns for each pulse, including last (12 bit)   |
| Video Camera          | Internal video camera (NTSC or PAL)   |
| Image capture         | Compatible with full Optech camera line (optional)  |
| Full waveform capture | 12-bit Optech IWD-2 Intelligent Waveform Digitizer<br>(optional)  |
| Data storage          | Removable solid state disk SSD (SATA II)  |
| Power requirements    | 28 V; 900 W;35 A(peak)  |
| Dimensions and weight | Sensor: 260 mm (w) x 190 mm (l) x 570 mm (h); 23 kg<br>Control rack: 650 mm (w) x 590 mm (l) x 530 mm (h);<br>53 kg |
| Operating temperature | -10°C to +35°C (with insulating jacket)   |
| Relative humidity     | 0-95% no-condensing   |

## Annex 2. NAMRIA Certificates of Reference Points Used

PLW-23







NAMRIA OFFICES: Main : Lawton Arenue, Fort Bonifaco, 1634 Taguig City, Philippines Tel. No.: (632) 810-4831 to 41 Branch : 421 Branca St. San Nicolas, 1010 Manila, Philippines, Tel. No. (632) 241-3494 to 98 www.namria.gov.ph

ISO 9001: 2008 CERTIFIED FOR MAPPING AND GEOSPATIAL INFORMATION MANAGEMENT

Figure A-2.1. PLW-23

# Annex 3. Baseline Processing Reports of Control Points used in the LIDAR Survey

| Project information |                                | Coordinate System |                 |
|---------------------|--------------------------------|-------------------|-----------------|
| Name:               |                                | Name:             | UTM             |
| Size:               |                                | Datum:            | PRS 92          |
| Modified:           | 10/12/2012 4:40:11 PM (UTC:-6) | Zone:             | 51 North (123E) |
| Time zone:          | Mountain Standard Time         | Geoid:            | EGMPH           |
| Reference number:   |                                | Vertical datum:   |                 |
| Description:        |                                |                   |                 |

#### **Baseline Processing Report**

| Processing | Summary |
|------------|---------|
|------------|---------|

| Observation              | From   | То       | Solution Type | H. Prec.<br>(Meter) | V. Prec.<br>(Meter) | Geodetic<br>Az. | Ellipsoid<br>Dist.<br>(Meter) | ∆Height<br>(Meter) |
|--------------------------|--------|----------|---------------|---------------------|---------------------|-----------------|-------------------------------|--------------------|
| PLW-23 PLW-<br>4030 (B1) | PLW-23 | PLW-4030 | Fixed         | 0.001               | 0.002               | 205°42'51"      | 769.753                       | 0.756              |
| PLW-23 PLW-<br>4030 (B2) | PLW-23 | PLW-4030 | Fixed         | 0.001               | 0.002               | 205°42'52"      | 769.751                       | 0.758              |
| PLW-23 PL-267<br>(B3)    | PLW-23 | PL-267   | Fixed         | 0.014               | 0.057               | 19°50'09"       | 49671.383                     | 24.118             |
| PLW-23 PLW-<br>4030 (B4) | PLW-23 | PLW-4030 | Fixed         | 0.001               | 0.002               | 205°42'54"      | 769.752                       | 0.745              |

#### Acceptance Summary

| Processed | Passed | Flag | P | Fail | Þ |
|-----------|--------|------|---|------|---|
| 4         | 4      | 0    |   | 0    |   |

Figure A-3.1. Baseline Processing Report - A

#### PLW-23 - PLW-4030 (11:45:04 AM-3:31:34 PM) (S1)

| Baseline observation:  | PLW-23 PLW-4030 (B1)                    |
|------------------------|---|
| Processed:             | 12/16/2015 2:07:32 PM                   |
| Solution type:         | Fixed                                   |
| Frequency used:        | Dual Frequency (L1, L2)                 |
| Horizontal precision:  | 0.001 m                                 |
| Vertical precision:    | 0.002 m                                 |
| RMS:                   | 0.000 m                                 |
| Maximum PDOP:          | 2.098                                   |
| Ephemeris used:        | Broadcast                               |
| Antenna model:         | NGS Absolute                            |
| Processing start time: | 11/20/2015 11:45:29 AM (Local: UTC+8hr) |
| Processing stop time:  | 11/20/2015 3:31:34 PM (Local: UTC+8hr)  |
| Processing duration:   | 03:46:05                                |
| Processing interval:   | 5 seconds                               |
|                        |   |

#### Vector Components (Mark to Mark)

| From:     | PLW-23        |           |                   |           |                   |
|-----------|---------------|-----------|-------------------|-----------|-------------------|
| G         | rid           | Lo        | cal               | Glo       | bal               |
| Easting   | 84385.264 m   | Latitude  | N10°05'19.52518"  | Latitude  | N10°05'15.04804"  |
| Northing  | 1117566.788 m | Longitude | E119°12'33.72062" | Longitude | E119°12'39.01413" |
| Elevation | 9.470 m       | Height    | 10.427 m          | Height    | 61.073 m          |

| То:        | PLW-4030      |        |                 |            |          |            |     |                   |
|------------|---------------|--------|-----------------|------------|----------|------------|-----|-------------------|
| G          | rid           |        | Loc             | al         |          |            | Glo | bal               |
| Easting    | 84042.662 m   | Latitu | ude             | N10°04'56  | 6.95146" | Latitude   |     | N10°04'52.47562"  |
| Northing   | 1116875.986 m | Long   | gitude          | E119°12'22 | 2.75168" | Longitude  |     | E119°12'28.04576" |
| Elevation  | 10.228 m      | Heig   | ht              | 1          | 1.183 m  | Height     |     | 61.835 m          |
| Vector     |               |        |                 |            |          |            |     |                   |
| ΔEasting   | -342.60       | 02 m   | NS Fwd Azimuth  |            |          | 205°42'51" | ΔX  | 231.869 m         |
| ΔNorthing  | -690.80       | 02 m   | Ellipsoid Dist. |            |          | 769.753 m  | ΔY  | 269.625 m         |
| ΔElevation | 0.75          | 58 m   | ∆Height         |            |          | 0.756 m    | ΔZ  | -682.686 m        |

#### Standard Errors

| Vector errors:            |         |                   |          |     |         |
|---------------------------|---------|-------------------|----------|-----|---------|
| σ ΔEasting                | 0.000 m | σ NS fwd Azimuth  | 0°00'00" | σΔΧ | 0.001 m |
| σ ΔNorthing               | 0.000 m | σ Ellipsoid Dist. | 0.000 m  | σΔΥ | 0.001 m |
| $\sigma \Delta Elevation$ | 0.001 m | σ ΔHeight         | 0.001 m  | σΔΖ | 0.000 m |

2

Figure A-3.2. Baseline Processing Report - B

| From:      | PLW-23        |                     |              |        |             |     |                   |
|------------|---------------|---------------------|--------------|--------|-------------|-----|-------------------|
| G          | rid           | Lo                  | cal          |        |             | Glo | bal               |
| Easting    | 84385.264 m   | Latitude            | N10°05'19.5  | 52518" | Latitude    |     | N10°05'15.04804"  |
| Northing   | 1117566.788 m | Longitude           | E119°12'33.7 | 72062" | Longitude   |     | E119°12'39.01413" |
| Elevation  | 9.470 m       | Height              | 10.          | .427 m | Height      |     | 61.073 m          |
| To:        | PL-267        |                     |              |        |             |     |                   |
| G          | rid           | Lo                  | cal          |        |             | Glo | bal               |
| Easting    | 101820.908 m  | Latitude            | N10°30'40.2  | 21529" | Latitude    |     | N10°30'35.64621"  |
| Northing   | 1164164.984 m | Longitude           | E119°21'48.0 | 02348" | Longitude   |     | E119°21'53.27911" |
| Elevation  | 33.463 m      | Height              | 34.          | .545 m | Height      |     | 84.611 m          |
| Vector     |               |                     |              |        |             |     |                   |
| ΔEasting   | 17435.64      | 4 m NS Fwd Azimuth  |              |        | 19°50'09"   | ΔX  | -10634.211 m      |
| ΔNorthing  | 46598.19      | 7 m Ellipsoid Dist. |              |        | 49671.383 m | ΔY  | -15515.024 m      |
| ΔElevation | 23.99         | 3 m <b>∆Height</b>  |              |        | 24.118 m    | ΔZ  | 45972.210 m       |

#### Vector Components (Mark to Mark)

#### Standard Errors

| Vector errors: |         |                   |          |     |         |
|----------------|---------|-------------------|----------|-----|---------|
| σ ΔEasting     | 0.004 m | σ NS fwd Azimuth  | 0°00'00" | σΔΧ | 0.013 m |
| σ ΔNorthing    | 0.005 m | σ Ellipsoid Dist. | 0.006 m  | σΔΥ | 0.026 m |
| σ ΔElevation   | 0.029 m | σ ΔHeight         | 0.029 m  | σΔΖ | 0.005 m |

#### Aposteriori Covariance Matrix (Meter<sup>2</sup>)

|   | х             | Y            | Z            |
|---|---------------|--------------|--------------|
| x | 0.0001625016  |              |              |
| Y | -0.0003217825 | 0.0006901336 |              |
| Z | -0.0000343902 | 0.0000615645 | 0.0000255690 |

Figure A-3.3. Baseline Processing Report – C

#### Data Acquisition Agency / Component Designation Name Affiliation Sub -Team PHIL-LIDAR 1 **Program Leader** ENRICO C. PARINGIT, D.ENG **UP-TCAGP** Data Acquisition Data Component ENGR. CZAR JAKIRI SARMIENTO **UP-TCAGP Component Leader** Project Leader – I Chief Science Research ENGR. CHRISTOPHER CRUZ **UP-TCAGP** Specialist (CSRS) Survey Supervisor LOVELY GRACIA ACUÑA **UP-TCAGP** Supervising Science **Research Specialist** (Supervising SRS) LOVELYN ASUNCION **UP-TCAGP FIELD TEAM** Research Associate (RA) JASMINE ALVIAR **UP-TCAGP LiDAR Operation** ENGR. LARAH KRISELLE RA **UP-TCAGP** PARAGAS GRACE SINADJAN RA **UP-TCAGP** Ground Survey, Data Download and Transfer RA JERIEL PAUL ALAMBAN, GEOL. **UP-TCAGP** PHILIPPINE AIR Airborne Security SSG. ARIES TORNO FORCE (PAF) ASIAN AEROSPACE **LiDAR Operation** CAPT. MARK TANGONAN CORPORATION Pilot (AAC) AAC CAPT. JUSTINE JOYA

#### Annex 4. The LiDAR Survey Team Composition

Hazard Mapping of the Philippines Using LIDAR (Phil-LIDAR 1)

# Annex 5. Data Transfer Sheets



Figure A-5.1. Data Transfer Sheet for Caramay Floodplain - A

|              | CERVER     | I OCATION | AL CONTRACT         | A ZNDACHAW  | IA Z:IDACIRAW<br>DATA | 4A ZIDACIRAW<br>DATA | VA Z:/DACH-AW | NA ZNDACIRAW | NA ZUDACIRAW | NA ZUDACIRAW   | NA ZIDACIRAW | NA ZIDACIRAW |               |               |               |                                      |   |  |  |
|--------------|------------|-----------|---------------------|-------------|-----------------------|----------------------|---------------|--------------|--------------|----------------|--------------|--------------|---------------|---------------|---------------|--------------------------------------|---|--|--|
|              | IGHT PLAN  |           | II KN               | N /91/      | 3/16/ N               | 5/13 P               | 6             | 2/16/        | 13/15        | 15             | CCIP         | 22/48/       |               |               |               |                                      |   |  |  |
|              | L FL       | ×         | ) Actua             | 21/22/16    | 21/22/18              | 13/13/1              | 13/1          | 22/21/2      | 13/13/       | 13/            | cicc         | 22/24        | 2             |               |               |                                      |   |  |  |
|              |            | OPERATO   | 10PLOG              | 1KB         | 1KB                   | 1KB                  | 1KB           | MA           | 140          |                | avi .        | IKB          | avi           |               |               |                                      |   |  |  |
|              | A STATUTE  | (CINOIIA) | Base Info<br>(.txt) | 1KB         | 1KB                   | 1KB                  | 1KB           | avia         |              | 1KB            | 1KB          | 1KB          | 1KB           |               |               |                                      |   |  |  |
|              |            | BASE 51   | BASE<br>et ATION(S) | 3.97        | 4.14                  | 8.03                 | £ 70          |              | 10.1         | 8.36           | 8.36         | 4.3          | 6.96          |               | 11            | 1                                    |   |  |  |
|              |            |           | DIGITIZER           |             | -                     | vol vite             |               | NA           | NA           | NA             | NA           | NA           | NA            |               |               | 14114                                |   |  |  |
|              |            | -         | RANGE               |             | 8.14                  | 2.53                 | 6.11          | 24.7         | 15.8         | 16             | 19.1         | 19           | 25.4          |               | the           | K                                    |   |  |  |
|              |            | -         | SSION LOG           | LOGS        | 10/74/33              | 34                   | AN            | NA           | NA           | NA             | NA           | NA           | NA            |               | Bow           | e ant                                |   |  |  |
| <b>SHEET</b> | 08/15      | -         | RAW PAIS            | GESICASI    | .81/13.3              | 4.34                 | NA            | NA           | NA           | NA             | AN<br>NA     | NA           | NA            | and hearth a  | Name AC       | Signature                            |   |  |  |
| A TRANSFEF   | ALAWAN 121 |           |                     | POS IMA     | 180 1                 | 65                   | 199           | 229          | 228          | 187            | 238          | 195          | 202           |               |               |                                      |   |  |  |
| DAT          | đ          | 11. 15.   |                     | OGS(MB)     | 991                   | 410                  | 209           | 619          | 667          | 280            | ADE          | 147          | 363           | ~             |               |                                      |   |  |  |
|              |            |           | S                   | IL (swath)  | 176/846               | 32                   | 18/218        | 2RF          | 004          | 2001           | 202          | 76           | 977           | NA            |               |                                      |   |  |  |
|              |            |           | RAWLA               | tput LAS KA | NA                    | NA                   | NA            |              | VN           | NA             | NA           | NA           | NA            | NA            |               |                                      |   |  |  |
|              |            |           |                     | SENSOR      | TANINI                | Even Nil             |               | EMINI        | EMINI        | SEMINI         | SEMINI       | GEMINI       | GEMINI        | GEMINI        |               | ALC L                                | A |  |  |
|              |            |           |                     | SION NAME   |                       | 2BLK42isIAs324A      | 2BLK42B325A   | 2BLK42HJ330A | 2BLK42I331A  | 2BLK42B40A332A | 2BLK42HJ334A | ZBLK42JK334B | 2BLK42HsL335A | 2BLK42PQR337A | Received from | Name C 'Yoo<br>Position<br>Signature | 7 |  |  |
|              |            |           |                     | Sim On and  |                       | 3513G                | 3517G         | 3537G        | 3541G        | 3545G          | 35536        | 3555G        | 35576         | 35656         |               |                                      |   |  |  |
|              |            |           | 1                   |             | FLIG                  | 0-Nov-15             | 1-Nov-15      | 6-Nov-15     | 7-Nov-15     | 0-Nov-15       | to Mou-15    | To Mourt5    | 1 Darie       | 2-Dor-15      |               |                                      |   |  |  |

Figure A-5.2. Data Transfer Sheet for Caramay Floodplain - B

# Annex 6. Flight Logs





Figure A-6.1. Flight Log for 2BLK42AES322A Mission



### Flight Log for 2BLK42ISLAS322B Mission

Figure A-6.2. Flight Log for 2BLK42ISLAS322B Mission

## Flight Log for 2BLK42isIAs324A Mission

| or: J ALMANEZ 2 ALTM Model: GEMIN 3 Mission Name: 4 Type: VFR 5<br>arogoron 8 Co-Pilot: A. Looco 9 Route: Puerto PRINCESA 17/pe: VFR 5<br>of 12 Aliport of Departure (Microfi City/Frovince): 12 Airport of Arrial (Air<br>of 2 ALTM PRINCE) 2010 al Engine Time: 12 Airport PRINCE 2010<br>Low doud coiling 1 (15 Total Engine Time: 16 Take off: 1<br>1457 0 Aircraft Tast Flight 0 LIDAR System Maintenance 5<br>20.5 Others 20.5 Others 20.5 Others 5<br>20.6 Nitres 0 Aircraft Tast Flight 0 Hild Adminetance 5<br>attom 20.0 Not Billable 20.5 Others 5<br>20.6 Nitres 0 Aircraft Tast Flight 0 Hild Adminetance 5<br>attom 7<br>20.6 Nitres 0 Aircraft Tast Flight 0 Hild Adminetance 5<br>attom 7<br>20.6 Nitres 0 Aircraft Tast Flight 0 Hild Adminetance 5<br>attom 7<br>20.6 Nitres 0 Phil-LIDAR Admin Activities 5<br>attom 7<br>Problem Problem 7<br>Problem 7<br>Problem 7<br>Problem 7<br>20.6 Nitres 0 Phil-LIDAR Admin Activities 5<br>20.6 Nitres 0 Phile 0 |                                 | Flight Log No.: 3 573               |
|---|---------------------------------|-------------------------------------|
| Approved by Acquigition Flight Certified by Problem Control of Arrival Attraction Province: 12 Airport of Arrival Attraction Control De parture (Airport Gity/Province): 12 Airport of Arrival Attraction Control De parture (Airport of Tayles Off: 12 Airport of Arrival Attraction Control De parture (Airport of Tayles Off: 12 Airport of Arrival Attraction Control De parture (Airport of Arrival Attraction Control De parture) (Arrow Control De Arrow Cont  | Aircraft Type: Cesnna T206H     | 6 Aircraft Identification: 907.2    |
| Index     In Ariport of De parture (Airport, Gity/Province):     In 2 Airport of Arrival (Airport, Gity/Province):       In Arrain off:     In 4 Engine Off:     In 2 Airport of Arrival (Airport, Gity/Province):       In Arrain off:     In 4 Engine Off:     In 5 Total Engine Time:     In 2 Airport of Arrival (Airport, Gity/Province):       In Arrain off:     In 4 Engine Off:     In 4 Engine Off:     In 4 Engine Off:     In 4 Engine Off:       In Arrain off:     In 4 Engine Off:     In 4 Engine     In 4 Engine     In 4 Engine       In Arrain Fight     O Arrain Fight     O Libras     Supplemente       20.0 And and Fight     O Arrain Fight     O Arrain Airbin Admin Admin Arrive     Supplemente       In Fight     O Others:     O Phil-IIDAR Admin Arrives     Supplemente       Intitions     O Others:     O Phil-IIDAR Admin Arrives     Supplemente       Intitions     O Others:     O Phil-IIDAR Admin Arrives     Supplemente       Intitions     Arranditions     Pilot-in-Continuente     Day  |                                 | )<br>k<br>                          |
| 14 Engine Off:     15 Total Engine Time:     16 Take off:     1       1457     14 20     14 20     20 5 Non Billable     20.0 Others       1451     20.0 Non Billable     20.0 Others     20.0 Non Billable     20.0 Cothers       20.0 Non Billable     20.0 Others     20.0 Non Billable     20.0 Others     50.0 Cothers       20.0 Non Billable     20.0 Others     20.0 Non Billable     20.0 Others     50.0 Cothers       20.0 Non Billable     20.0 Non Billable     20.0 Others     50.0 Cothers     50.0 Cothers       21 Remarks     0 Nicreft Rast Flight     0 Hill-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phil-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phil-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phil-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phil-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phil-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phil-HDAR Admin Activities     50.0 Cothers       18 fight     0 Others:     0 Phile     0 Phile     50.0 Cothers   | port, Gty/Province):<br>NSESP   |                                     |
| tow     doud     celltrQ       ton     doud     celltrQ       20.b Non Billable     20.c Others     20.c Others       20.b Non Billable     20.c Others     Successful       20.b Non Billable     0 Atriant Test Filght     0 LIDAR System MaIntenance       0. AKC Admin Filght     0 Atriantenance     Supplemence       0. Atriantenance     0 Others:     Douglemence       0. Others:     0 Phil-LIDAR Admin Activities     Doy       n Filght     0 Others:     Dop       Approved by     Acquisition Filght Certified by     Pilot-in-Confinance   | 7 Landing: 1452th               | 18 Total Flight Time:<br>4 +10      |
| don 20.0 Non Billable 20.0 Others 20.0 Others 20.0 Non Billable 20.0 Others 20.0 Non Billable 20.0 Others Supplemente tit 0 Aircraft Tast Flight 0 LiDAR Admin Activities Supplemente tit 0 Others:   |                                 |                                     |
| 20.b Non Billable     20.c Others     Successful       an Flight     O     Aircraft Test Flight     O       it     O     Aircraft Test Flight     O       it     O     Aircraft Test Flight     O       ast Flight     O     Others.     O       an Flight     O     Introve tothers.     D       an other     Introve tother     Introve tother     Introve tother   |                                 |                                     |
| tit o Ad Admin Fight o Arreat Maintenance or a are<br>ss Flight o Others. o Phi-UDAR Admin Activities or a or<br>in Flight o Others. o Phi-UDAR Admin Activities or a or<br>ohthous<br>Problem<br>Othem<br>Internations<br>Approved by Acquisition Flight Certified by Pilot-in-Connand   | l Flight,<br>Many Flights Blk42 | A and covered handa                 |
| Aproved by Aquisition Flight Certified by Plot-in-Connand   | l clands. Two sets              | of POS and range data               |
| Problem<br>cobient<br>roblem<br>Jern<br>Approved by Acquisition Flight Certified by Pilot-in-Connand  |                                 |                                     |
| roblem<br>tern<br>Approved by Acquisition Flight Certified by Pilot-in-Confinant  |                                 |                                     |
| Approved by Acquisition Flight Certified by Pilot-in-Confinant  |                                 |                                     |
| the Cot Romires. Phr M. Tangonan<br>intertaine Stante over Printed Name<br>resentative) (PAR Representative)  | UDAR Operator                   | Aircraft Mechanic/ IIDAR Technician |

Figure A-6.3. Flight Log for 2BLK42islAs324A Mission

## Flight Log for 2BLK42B325A Mission

| ata Acquisition Flight Log | LIDAR Operator: Mcs adultures 2 | Pilot:         M. THNLONAN         8 Co-Pilo           0 Date:         11 | 3 Engine On: 0745 14 Engin     | 9 Weather | 0 Flight Classification | 0.a Billable 20.b No           | Acquisition Flight     Acquisition Flight     System Test Flight     Calibration Flight               | <ul> <li>2 Problems and Solutions</li> <li>0 Weather Problem</li> <li>5 System Problem</li> </ul> | o Aucrart Problem<br>o Pilot Problem<br>o Others: | Acquisition Flight Approved by<br>Adv Approved by<br>Adv Approved by<br>Signature over Printed Name<br>(End User Representative) |
|----------------------------|---------------------------------|---|--------------------------------|-----------|-------------------------|--------------------------------|---|---|---|--|
|                            | 2 ALTM Model: GEM               | ot: R. LAACO<br>2 Airport of Departure (                                  | ie Off:                        | vdy       |                         | on Billable                    | Aircraft Test Flight<br>AAC Admin Flight<br>Others:   |   |   | Acquisition Flight Certi<br>A Comite<br>Signature over Printed N   |
|                            | 3 Mission Name: JOLE 4263       | 9 Route: 7Ps - 7P.<br>(Airport, City/Province):                           | 15 Total Engine Time:          |           |                         | 20.c Others                    | <ul> <li>LiDAR System Mainten</li> <li>Aircraft Maintenance</li> <li>Phil-LiDAR Admin Acti</li> </ul> | 199 S   |   | fied by Pilot-in-C   |
|                            | 4 Type: VFR                     | 5<br>12 Airport of Arrix  | 16 Take off: 1                 |           | 21 Rem                  | hans 1.                        | nance creshre<br>led. s<br>vities data  |   |   | Command<br>Marcenter<br>over Printed Name  |
|                            | 5 Aircraft Type: CesnnaT206H    | al (Airport. City/Province):  | Nurente Unicrea<br>17 Landing: |           | arks                    | fed 3 lines over Bukyrk wit    | d & Task Dead Error was<br>mark & Arnsiectory with range<br>& are not praceable. No heli              |   |   | Lidar Operator   |
| Flight Log No.: 35136      | 6 Aircraft Identification: 7022 |   | 18 Total Flight Time:          |           |                         | the wids due to clouds . Diops | appriared. There is difference of<br>AR. Level 2 lines has no POS                                     |   |   | Aircraft Mechanic/ Technician  |

Figure A-6.4. Flight Log for 2BLK42B325A Mission

#### Flight Log for 2BLK42B332A Mission



Figure A-6.5. Flight Log for 2BLK42B332A Mission

# Annex 7. Flight Status Report

CARAMAY FLOODPLAIN (November 18-28, 2015)

| FLIGHT<br>NO. | AREA                | MISSION         | OPERATOR     | DATE<br>FLOWN | REMARKS   |
|---------------|---------------------|-----------------|--------------|---------------|---|
| 3505G         | BLK42eA,<br>42A     | 2BLK42AEs322A   | MCE Baliguas | 18-Nov-15     | Voids on<br>mountainous part<br>of 42eA; covered<br>42A voids |
| 3507G         | BLK42eA             | 2BLK42islAs322B | JM Almalvez  | 18-Nov-15     | Covered 42eA  |
| 3513G         | BLK42eA,<br>islands | 2BLK42islAs324A | JM Almalvez  | 20-Nov-15     | Covered 42eA  |
| 3517G         | BLK42eB             | 2BLK42B325A     | MCE Baliguas | 21-Nov-15     | Covered 42eB  |
| 3545G         | BLK42eB,<br>BLK40A  | 2BLK42B40A332A  | JM Almalvez  | 28-Nov-15     | Surveyed BLK42eB<br>and moved to<br>BLK40A                    |

LAS/SWATH BOUNDARIES PER MISSION FLIGHTFLIGHT LOG NO. 3505GScan Freq: 50 kHzAREA: BLOCK 42eA & 42AScan Angle: 15 degMISSION NAME: 2BLK42AES322AAlt: 1200 m



Figure A-7.1. Swath for Flight No. 3505G

FLIGHT LOG NO. 3507G AREA: BLOCK 42eA MISSION NAME: 2BLK42ISLAS322B Scan Freq: 50 kHz Scan Angle: 15 deg Alt: 1200 m



Figure A-7.2. Swath for Flight No. 3507G

FLIGHT LOG NO. 3513G AREA: BLOCK 42eA MISSION NAME: 2BLK42islAs324A Scan Freq: 50 kHz Scan Angle: 15 deg Alt: 1200 m



Figure A-7.4. Swath for Flight No. 3513G

FLIGHT LOG NO. 3517G AREA: BLOCK 42eAB MISSION NAME: 2BLK42B325A Scan Freq: 50 kHz Scan Angle: 15 deg Alt: 1200 m



Figure A-7.5. Swath for Flight No. 3517G

#### FLIGHT LOG NO. 3545G AREA: BLOCK 42eAB & 40A MISSION NAME: 2BLK42B332A

Scan Freq: 50 kHz Scan Angle: 15 deg Alt: 1200 m



Figure A-7.6. Swath for Flight No. 3545G
## Annex 8. Mission Summary Report

| Flight Area                                   | Palawan Reflights   |  |  |  |  |
|---|---|--|--|--|--|
| Mission Name                                  | Blk42eA   |  |  |  |  |
| Inclusive Flights                             | 3505G, 3507G  |  |  |  |  |
| Range data size                               | 30.7 GB   |  |  |  |  |
| Base data size                                | 16.18 MB  |  |  |  |  |
| POS   | 402 MB  |  |  |  |  |
| Image   | NA  |  |  |  |  |
| Transfer date                                 | December 8, 2015  |  |  |  |  |
|   |   |  |  |  |  |
| Solution Status                               |   |  |  |  |  |
| Number of Satellites (>6)                     | Yes   |  |  |  |  |
| PDOP (<3)                                     | Yes   |  |  |  |  |
| Baseline Length (<30km)                       | No  |  |  |  |  |
| Processing Mode (<=1)                         | Yes   |  |  |  |  |
|   |   |  |  |  |  |
| Smoothed Performance Metrics (in cm)          |   |  |  |  |  |
| RMSE for North Position (<4.0 cm)             | 1.52  |  |  |  |  |
| RMSE for East Position (<4.0 cm)              | 1.72  |  |  |  |  |
| RMSE for Down Position (<8.0 cm)              | 4.29  |  |  |  |  |
|   |   |  |  |  |  |
| Boresight correction stdev (<0.001deg)        | 0.000835  |  |  |  |  |
| IMU attitude correction stdev (<0.001deg)     | 0.090429  |  |  |  |  |
| GPS position stdev (<0.01m)                   | 0.0271  |  |  |  |  |
|   |   |  |  |  |  |
| Minimum % overlap (>25)                       | 36.93%  |  |  |  |  |
| Ave point cloud density per sq.m. (>2.0)      | 4.70  |  |  |  |  |
| Elevation difference between strips (<0.20 m) | Yes   |  |  |  |  |
|   |   |  |  |  |  |
| Number of 1km x 1km blocks                    | 142   |  |  |  |  |
| Maximum Height                                | 514.64 m  |  |  |  |  |
| Minimum Height                                | 50.90 m   |  |  |  |  |
|   |   |  |  |  |  |
| Classification (# of points)                  |   |  |  |  |  |
| Ground  | 30,345,934  |  |  |  |  |
| Low vegetation                                | 27,828,311  |  |  |  |  |
| Medium vegetation                             | 157,391,700   |  |  |  |  |
| High vegetation                               | 210,127,503   |  |  |  |  |
| Building                                      | 3,839,873   |  |  |  |  |
| Ortophoto                                     | No  |  |  |  |  |
| Processed by                                  | Engr. Jennifer Saguran, Engr. Analyn Naldo,<br>Engr. Justine Francisco, Melissa |  |  |  |  |

Table A-8.1. Mission Summary Report for Mission Blk42eA



Figure A-8.1. Solution Status



Figure A-8.2. Smoothed Performance Metrics Parameters



Figure A-8.3. Best Estimated Trajectory



Figure A-8.4 Coverage of LiDAR data



Figure A-8.5. Image of data overlap



Figure A-8.6. Density map of merged LiDAR data



Figure A-8.7. Elevation difference between flight lines

| Flight Area                                   | Palawan Reflights   |  |  |  |
|---|---|--|--|--|
| Mission Name                                  | Blk42eB   |  |  |  |
| Inclusive Flights                             | 3545G   |  |  |  |
| Range data size                               | 15.8 GB   |  |  |  |
| Base data size                                | 10.1 MB   |  |  |  |
| POS   | 228 MB  |  |  |  |
| Image   | NA  |  |  |  |
| Transfer date                                 | January 4, 2016   |  |  |  |
|   |   |  |  |  |
| Solution Status                               |   |  |  |  |
| Number of Satellites (>6)                     | No  |  |  |  |
| PDOP (<3)                                     | Yes   |  |  |  |
| Baseline Length (<30km)                       | Yes   |  |  |  |
| Processing Mode (<=1)                         | Yes   |  |  |  |
|   |   |  |  |  |
| Smoothed Performance Metrics (in cm)          |   |  |  |  |
| RMSE for North Position (<4.0 cm)             | 1.26  |  |  |  |
| RMSE for East Position (<4.0 cm)              | 1.12  |  |  |  |
| RMSE for Down Position (<8.0 cm)              | 1.89  |  |  |  |
|   |   |  |  |  |
| Boresight correction stdev (<0.001deg)        | 0.020777  |  |  |  |
| IMU attitude correction stdev (<0.001deg)     | 0.017523  |  |  |  |
| GPS position stdev (<0.01m)                   | 0.0279  |  |  |  |
|   |   |  |  |  |
| Minimum % overlap (>25)                       | 21.10%  |  |  |  |
| Ave point cloud density per sq.m. (>2.0)      | 4.94  |  |  |  |
| Elevation difference between strips (<0.20 m) | Yes   |  |  |  |
|   |   |  |  |  |
| Number of 1km x 1km blocks                    | 84  |  |  |  |
| Maximum Height                                | 547.79 m  |  |  |  |
| Minimum Height                                | 50.86 m   |  |  |  |
|   |   |  |  |  |
| Classification (# of points)                  |   |  |  |  |
| Ground  | 8,276,887   |  |  |  |
| Low vegetation                                | 4,050,735   |  |  |  |
| Medium vegetation                             | 48,822,536  |  |  |  |
| High vegetation                               | 142,807,210   |  |  |  |
| Building                                      | 1,882,543   |  |  |  |
|   |   |  |  |  |
| Ortophoto                                     | No  |  |  |  |
| Processed by                                  | Engr. Kenneth Solidum,<br>Engr. Merven Matthew Nating, Denise |  |  |  |

## Table A-8.2. Mission Summary Report for Mission Blk42eB



Figure A-8.8. Solution Status



Figure A-8.9. Smoothed Performance Metrics Parameters



Figure A-8.10. Best Estimated Trajectory



Figure A-8.11. Coverage of LiDAR data



Figure A-8.12. Image of data overlap



Figure A-8.13. Density map of merged LiDAR data



Figure A-8.14. Elevation difference between flight lines

# Annex 9. Caramay Model Basin Parameters

|          | SCS                            | CURVE NUMB      | ER LOSS               | CLARK UNIT HYDROGRAPH<br>TRANSFORM |                             |  |
|----------|--------------------------------|-----------------|-----------------------|------------------------------------|-----------------------------|--|
| Subbasin | Initial<br>Abstraction<br>(MM) | Curve<br>Number | Imperviousness<br>(%) | Time of<br>Concentration<br>(HR)   | Storage<br>Coefficient (HR) |  |
| W1000    | 10.35                          | 55              | 0                     | 0.86982                            | 1.4195                      |  |
| W1010    | 10.35                          | 55              | 0                     | 1.0201                             | 1.6649                      |  |
| W1020    | 10.35                          | 55              | 0                     | 0.52261                            | 0.85289                     |  |
| W1030    | 10.35                          | 55              | 0                     | 1.1292                             | 1.8428                      |  |
| W1040    | 10.52                          | 54.694          | 0                     | 1.2456                             | 2.0327                      |  |
| W1050    | 10.35                          | 55              | 0                     | 1.417                              | 2.3126                      |  |
| W1060    | 5.8914                         | 68.311          | 0                     | 0.70784                            | 1.1552                      |  |
| W1070    | 4.65                           | 73              | 0                     | 0.41522                            | 0.67764                     |  |
| W1080    | 6.5898                         | 65.838          | 0                     | 0.71641                            | 1.1692                      |  |
| W1090    | 5.2937                         | 70.58           | 0                     | 0.81371                            | 1.328                       |  |
| W1100    | 4.9577                         | 71.923          | 0                     | 1.0401                             | 1.6975                      |  |
| W1120    | 10.481                         | 54.786          | 0                     | 1.4702                             | 2.3993                      |  |
| W1130    | 7.6444                         | 62.425          | 0                     | 0.98729                            | 1.6113                      |  |
| W1140    | 4.6665                         | 73.129          | 0                     | 0.53562                            | 0.87413                     |  |
| W1150    | 4.9001                         | 72.159          | 0                     | 0.91066                            | 1.4862                      |  |
| W1160    | 11.547                         | 52.377          | 0                     | 1.2148                             | 1.9826                      |  |
| W1170    | 8.5542                         | 59.753          | 0                     | 1.6172                             | 2.6393                      |  |
| W1180    | 8.9611                         | 58.631          | 0                     | 1.7314                             | 2.8257                      |  |
| W1190    | 12.285                         | 50.83           | 0                     | 1.5935                             | 2.6007                      |  |
| W1200    | 13.75                          | 48              | 0                     | 1.3606                             | 2.2205                      |  |
| W1210    | 10.35                          | 55              | 0                     | 1.1233                             | 1.8332                      |  |
| W1220    | 10.35                          | 55              | 0                     | 1.0601                             | 1.7301                      |  |
| W1240    | 12.763                         | 49.877          | 0                     | 1.7552                             | 2.8645                      |  |
| W1250    | 8.9285                         | 58.719          | 0                     | 1.9121                             | 3.1205                      |  |
| W620     | 10.35                          | 55              | 0                     | 1.5402                             | 2.5137                      |  |
| W630     | 10.35                          | 55              | 0                     | 1.4925                             | 2.4358                      |  |
| W640     | 10.35                          | 55              | 0                     | 1.0837                             | 1.7687                      |  |
| W650     | 10.35                          | 55              | 0                     | 1.355                              | 2.2113                      |  |
| W660     | 10.35                          | 55              | 0                     | 0.91128                            | 1.4872                      |  |
| W670     | 10.35                          | 55              | 0                     | 0.18442                            | 0.30098                     |  |

Table A-9.1 Caramay Model Basin Parameters

| SCS CURVE NUMBER LOSS |                                |                 | CLARK UNIT HYDROGRAPH<br>TRANSFORM |                                  |                             |
|-----------------------|--------------------------------|-----------------|------------------------------------|----------------------------------|-----------------------------|
| Subbasin              | Initial<br>Abstraction<br>(MM) | Curve<br>Number | Imperviousness<br>(%)              | Time of<br>Concentration<br>(HR) | Storage<br>Coefficient (HR) |
| W680                  | 10.35                          | 55              | 0                                  | 0.84209                          | 1.3743                      |
| W690                  | 10.35                          | 55              | 0                                  | 1.1179                           | 1.8244                      |
| W700                  | 10.35                          | 55              | 0                                  | 0.68189                          | 1.1128                      |
| W710                  | 10.35                          | 55              | 0                                  | 0.29086                          | 0.47469                     |
| W720                  | 10.35                          | 55              | 0                                  | 1.4927                           | 2.4361                      |
| W730                  | 10.35                          | 55              | 0                                  | 1.2105                           | 1.9756                      |
| W740                  | 10.35                          | 55              | 0                                  | 0.97445                          | 1.5903                      |
| W750                  | 10.35                          | 55              | 0                                  | 0.48973                          | 0.79925                     |
| W760                  | 10.35                          | 55              | 0                                  | 0.69128                          | 1.1282                      |
| W770                  | 10.35                          | 55              | 0                                  | 1.5458                           | 2.5227                      |
| W780                  | 10.35                          | 55              | 0                                  | 2.2271                           | 3.6347                      |
| W790                  | 10.35                          | 55              | 0                                  | 1.4178                           | 2.3139                      |
| W800                  | 10.35                          | 55              | 0                                  | 1.1838                           | 1.932                       |
| W810                  | 10.35                          | 55              | 0                                  | 0.74586                          | 1.2172                      |
| W820                  | 10.35                          | 55              | 0                                  | 0.87134                          | 1.422                       |
| W830                  | 10.35                          | 55              | 0                                  | 1.2526                           | 2.0442                      |
| W840                  | 10.35                          | 55              | 0                                  | 1.0851                           | 1.7709                      |
| W850                  | 10.35                          | 55              | 0                                  | 0.83324                          | 1.3599                      |
| W860                  | 10.35                          | 55              | 0                                  | 1.5167                           | 2.4753                      |
| W870                  | 10.35                          | 55              | 0                                  | 0.94476                          | 1.5418                      |
| W880                  | 10.35                          | 55              | 0                                  | 0.60293                          | 0.98398                     |
| W890                  | 10.35                          | 55              | 0                                  | 0.62683                          | 1.023                       |
| W900                  | 10.35                          | 55              | 0                                  | 0.42838                          | 0.69912                     |
| W910                  | 10.35                          | 55              | 0                                  | 1.5868                           | 2.5897                      |
| W920                  | 10.35                          | 55              | 0                                  | 1.259                            | 2.0548                      |
| W930                  | 10.35                          | 55              | 0                                  | 0.92237                          | 1.5053                      |
| W940                  | 10.629                         | 54.439          | 0                                  | 0.9038                           | 1.475                       |
| W950                  | 9.6175                         | 56.906          | 0                                  | 1.1887                           | 1.9399                      |
| W960                  | 6.6292                         | 65.704          | 0                                  | 1.2886                           | 2.103                       |
| W970                  | 11.145                         | 53.262          | 0                                  | 0.8643                           | 1.4105                      |
| W980                  | 13.123                         | 49.182          | 0                                  | 1.3161                           | 2.1479                      |
| W990                  | 10.873                         | 53.876          | 0                                  | 1.473                            | 2.4039                      |

# Annex 10. Caramay Model Reach Parameters

|       | MUSKINGUM CUNGE CHANNEL ROUTING |          |           |                    |  |  |  |
|-------|---------------------------------|----------|-----------|--------------------|--|--|--|
| REACH | Length (M) Slope(M/M)           |          | Shape     | Side Slope (xH:1V) |  |  |  |
| R110  | 1759.2                          | 0.001206 | Trapezoid | 1                  |  |  |  |
| R120  | 339.71                          | 0.001206 | Trapezoid | 1                  |  |  |  |
| R1270 | 3050.8                          | 0.000697 | Trapezoid | 1                  |  |  |  |
| R140  | 729.41                          | 0.011412 | Trapezoid | 1                  |  |  |  |
| R170  | 3530.9                          | 0.016276 | Trapezoid | 1                  |  |  |  |
| R180  | 757.7                           | 0.039189 | Trapezoid | 1                  |  |  |  |
| R190  | 1269.1                          | 0.039189 | Trapezoid | 1                  |  |  |  |
| R200  | 1289.8                          | 0.020226 | Trapezoid | 1                  |  |  |  |
| R250  | 348.7                           | 0.022026 | Trapezoid | 1                  |  |  |  |
| R260  | 435.27                          | 0.022026 | Trapezoid | 1                  |  |  |  |
| R280  | 764.68                          | 0.020461 | Trapezoid | 1                  |  |  |  |
| R30   | 120.71                          | 0.12382  | Trapezoid | 1                  |  |  |  |
| R300  | 2099.7                          | 0.020461 | Trapezoid | 1                  |  |  |  |
| R330  | 947.4                           | 0.000417 | Trapezoid | 1                  |  |  |  |
| R350  | 1015.3                          | 0.007081 | Trapezoid | 1                  |  |  |  |
| R370  | 1048.1                          | 0.014842 | Trapezoid | 1                  |  |  |  |
| R380  | 649.41                          | 0.099429 | Trapezoid | 1                  |  |  |  |
| R400  | 1587.8                          | 0.021124 | Trapezoid | 1                  |  |  |  |
| R410  | 2156.5                          | 0.002115 | Trapezoid | 1                  |  |  |  |
| R420  | 537.7                           | 0.012509 | Trapezoid | 1                  |  |  |  |
| R450  | 1239.1                          | 0.012509 | Trapezoid | 1                  |  |  |  |
| R470  | 1177.4                          | 0.021773 | Trapezoid | 1                  |  |  |  |
| R480  | 1311.2                          | 0.008402 | Trapezoid | 1                  |  |  |  |
| R50   | 417.28                          | 0.029308 | Trapezoid | 1                  |  |  |  |
| R500  | 664.77                          | 0.002521 | Trapezoid | 1                  |  |  |  |
| R530  | 798.11                          | 0.008402 | Trapezoid | 1                  |  |  |  |
| R540  | 1368.1                          | 0.006722 | Trapezoid | 1                  |  |  |  |
| R550  | 1243                            | 0.032333 | Trapezoid | 1                  |  |  |  |
| R570  | 2873.9                          | 0.002521 | Trapezoid | 1                  |  |  |  |
| R70   | 755.98                          | 0.030927 | Trapezoid | 1                  |  |  |  |
| R90   | 311.42                          | 0.017823 | Trapezoid | 1                  |  |  |  |

Table A-10.1 Caramay Model Reach Parameters

# Annex 11. Caramay Flood Validation Data

| Point  | Point Validation Coordinates |           | Model Validation   |       |       |         | Rain                |         |
|--------|------------------------------|-----------|--------------------|-------|-------|---------|---------------------|---------|
| Number | Latitude                     | Longitude | Var (m) Points (m) | Error | Event | Date    | Return/<br>Scenario |         |
| 1      | 10.17856                     | 119.2325  | 0.03               | 1.36  | 1.33  | Quedan  | Dec. 2005           | 25-Year |
| 2      | 10.17987                     | 119.2294  | 0.04               | 1.15  | 1.11  |         | 2005                | 25-Year |
| 3      | 10.17997                     | 119.2314  | 0.14               | 0.5   | 0.36  | Quedan  | 2005                | 25-Year |
| 4      | 10.18016                     | 119.2323  | 0.22               | 0.7   | 0.48  | Quedan  | 2005                | 25-Year |
| 5      | 10.18017                     | 119.2322  | 0.19               | 1.36  | 1.17  | Quedan  | 2005                | 25-Year |
| 6      | 10.18026                     | 119.2323  | 0.19               | 0.86  | 0.67  | Quedan  | 2005                | 25-Year |
| 7      | 10.1803                      | 119.2288  | 0.31               | 1.1   | 0.79  |         | 2005                | 25-Year |
| 8      | 10.18033                     | 119.2329  | 0.06               | 1.75  | 1.69  | Quedan  | 2005                | 25-Year |
| 9      | 10.18057                     | 119.2328  | 0.11               | 0.9   | 0.79  | Quedan  |                     | 25-Year |
| 10     | 10.18076                     | 119.2314  | 0.09               | 0.88  | 0.79  |         | 2005                | 25-Year |
| 11     | 10.18084                     | 119.2289  | 0.03               | 0.3   | 0.27  |         | 2005                | 25-Year |
| 12     | 10.18082                     | 119.2358  | 0.05               | 0.5   | 0.45  | Quedan  | Dec. 18,<br>2005    | 25-Year |
| 13     | 10.18088                     | 119.2301  | 0.06               | 0.6   | 0.54  | Quedan  | 2005                | 25-Year |
| 14     | 10.18094                     | 119.231   | 0.34               | 0.95  | 0.61  | Quedan  | 2005                | 25-Year |
| 15     | 10.18094                     | 119.231   | 0.34               | 1.31  | 0.97  | Quedan  | 2005                | 25-Year |
| 16     | 10.18094                     | 119.231   | 0.34               | 1.14  | 0.8   | Quedan  | Dec. 18,<br>2005    | 25-Year |
| 17     | 10.18091                     | 119.2372  | 0.03               | 0.75  | 0.72  | Quedan  | Dec. 2005           | 25-Year |
| 18     | 10.18096                     | 119.2343  | 0.43               | 0.65  | 0.22  | Quedan  | Dec. 18,<br>2005    | 25-Year |
| 19     | 10.18102                     | 119.2322  | 0.35               | 1.1   | 0.75  | Quedan  | 2005                | 25-Year |
| 20     | 10.18108                     | 119.2322  | 0.19               | 0.3   | 0.11  | Quedan  | Dec. 2005           | 25-Year |
| 21     | 10.18109                     | 119.234   | 0.13               | 1.09  | 0.96  | Quedan  | Dec. 2005           | 25-Year |
| 22     | 10.18132                     | 119.2337  | 0.18               | 0.4   | 0.22  | Quedan  | Dec. 2005           | 25-Year |
| 23     | 10.18144                     | 119.2314  | 0.37               | 1     | 0.63  |         | 2005                | 25-Year |
| 24     | 10.18158                     | 119.2373  | 0.03               | 0     | -0.03 |         |                     | 25-Year |
| 25     | 10.18175                     | 119.2343  | 0.03               | 0.4   | 0.37  | Quedan  | Dec. 2005           | 25-Year |
| 26     | 10.18212                     | 119.2312  | 0.45               | 1.2   | 0.75  |         | Dec. 2005           | 25-Year |
| 27     | 10.18219                     | 119.2382  | 0.2                | 0.2   | 0     | Yolanda | Nov. 2013           | 25-Year |
| 28     | 10.18235                     | 119.234   | 0.03               | 0.55  | 0.52  | Quedan  | Dec. 2005           | 25-Year |
| 29     | 10.18285                     | 119.2319  | 0.03               | 1.3   | 1.27  | Yolanda | Nov. 2013           | 25-Year |

Table A-11.1 Caramay Flood Validation Data

| Point  | Validation | Coordinates | Model   | Validation |       |        |           | Rain                |
|--------|------------|-------------|---------|------------|-------|--------|-----------|---------------------|
| Number | Latitude   | Longitude   | Var (m) | Points (m) | Error | Event  | Date      | Return/<br>Scenario |
| 30     | 10.18458   | 119.2337    | 0.04    | 0.35       | 0.31  | Quedan | Dec. 2005 | 25-Year             |
| 31     | 10.18595   | 119.2327    | 0.1     | 0.36       | 0.26  | Quedan | Dec. 2005 | 25-Year             |
| 32     | 10.18669   | 119.2327    | 0.21    | 1.4        | 1.19  | Quedan | Dec. 2005 | 25-Year             |
| 33     | 10.18826   | 119.2317    | 0.12    | 0.97       | 0.85  | Quedan | Dec. 2005 | 25-Year             |
| 34     | 10.18846   | 119.2321    | 0.51    | 1.07       | 0.56  | Quedan | Dec. 2010 | 25-Year             |
| 35     | 10.18893   | 119.2314    | 1.09    | 1.12       | 0.03  | Quedan | Dec. 2007 | 25-Year             |
| 36     | 10.18895   | 119.2319    | 1.03    | 0.96       | -0.07 | Quedan | Dec. 2008 | 25-Year             |
| 37     | 10.1893    | 119.2295    | 0.7     | 0.92       | 0.22  | Quedan | Dec. 2006 | 25-Year             |
| 38     | 10.18955   | 119.2317    | 1.1     | 0.55       | -0.55 | Quedan | Dec. 2009 | 25-Year             |
| 39     | 10.18968   | 119.2304    | 1.26    | 1.71       | 0.45  | Quedan | Dec. 2015 | 25-Year             |
| 40     | 10.18976   | 119.2308    | 0.85    | 1.21       | 0.36  | Quedan | Dec. 2014 | 25-Year             |
| 41     | 10.18992   | 119.2292    | 0.82    | 1          | 0.18  | Quedan | Dec. 2005 | 25-Year             |
| 42     | 10.19039   | 119.2311    | 0.95    | 1.51       | 0.56  | Quedan | Dec. 2013 | 25-Year             |
| 43     | 10.1905    | 119.2321    | 1.35    | 1.32       | -0.03 | Quedan | Dec. 2011 | 25-Year             |
| 44     | 10.19057   | 119.2282    | 0.23    | 0          | -0.23 |        |           | 25-Year             |
| 45     | 10.19056   | 119.2317    | 1.42    | 1.26       | -0.16 | Quedan | Dec. 2012 | 25-Year             |
| 46     | 10.19107   | 119.2273    | 0.03    | 0          | -0.03 |        |           | 25-Year             |
| 47     | 10.19127   | 119.2279    | 0.96    | 0          | -0.96 |        |           | 25-Year             |
| 48     | 10.19143   | 119.2265    | 0.03    | 0          | -0.03 |        |           | 25-Year             |
| 49     | 10.19188   | 119.2262    | 0.03    | 0          | -0.03 |        |           | 25-Year             |

## Annex 12. Phil-LiDAR 1 UPLB Team Composition

#### **Project Leader**

Asst. Prof. Edwin R. Abucay (CHE, UPLB)

### **Project Staffs/Study Leaders**

Asst. Prof. Efraim D. Roxas (CHE, UPLB) Asst. Prof. Joan Pauline P. Talubo (CHE, UPLB) Ms. Sandra Samantela (CHE, UPLB) Dr. Cristino L. Tiburan (CFNR, UPLB) Engr. Ariel U. Glorioso (CEAT, UPLB) Ms. Miyah D. Queliste (CAS, UPLB) Mr. Dante Gideon K. Vergara (SESAM, UPLB)

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#### **Information Systems Analyst** Jan Martin C. Magcale

### **Project Assistants**

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